

CROCO

Coastal and Regional Ocean COmmunity model

Sediment modeling

Implementation and use within CROCO

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https://croco-ocean.gitlabpages.inria.fr/croco_doc

Outline

Ocean dynamics and sediment
Wave averaged equations
Bottom boundary layer

Models and features

Implementation in CROCO :
Equations
Code structure
Model Options

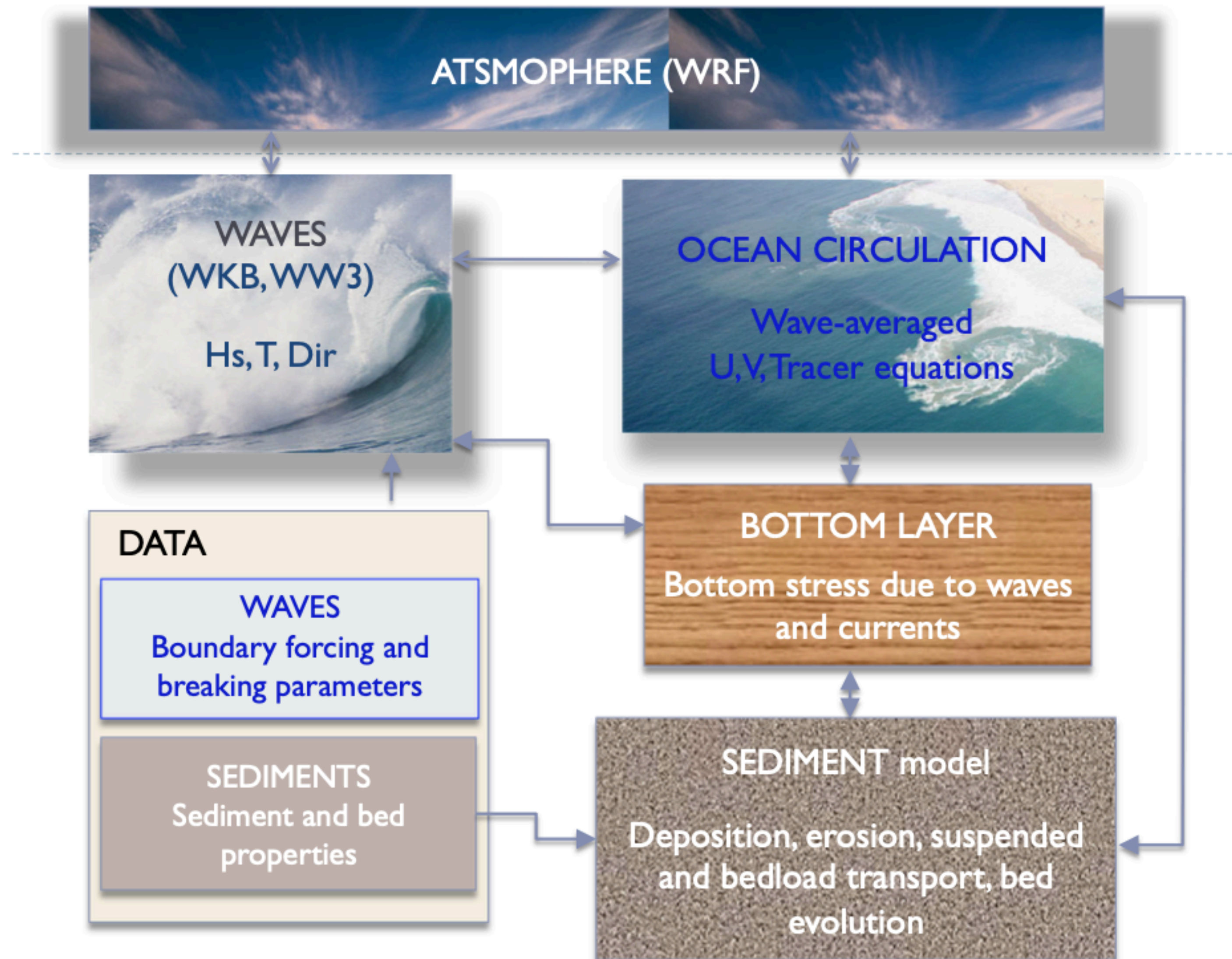
Options, parameters and input files

Examples

Ocean dynamics and sediment

Dynamics and sediment

Overview



Ocean dynamics and sediment

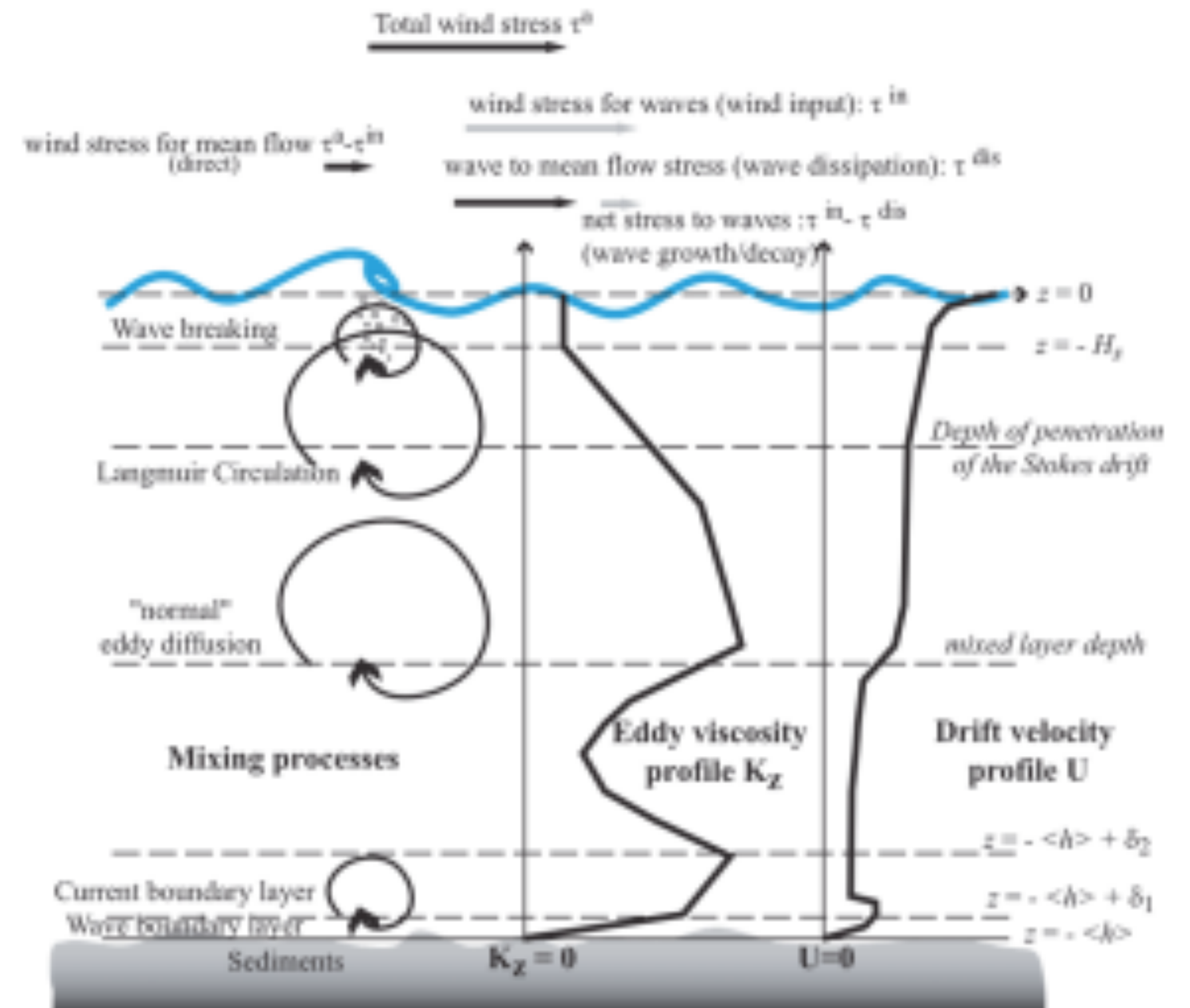
Waves averaged equations

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} + w \frac{\partial \mathbf{u}}{\partial z} + f \hat{\mathbf{z}} \times \mathbf{u} - \nabla \phi + \mathbf{F} = \nabla \kappa + \mathbf{J} + F^w$$

$$\frac{\partial \phi}{\partial z} + \frac{g\rho}{\rho_0} = -\frac{\partial \kappa}{\partial z} + K$$

$$\nabla \mathbf{u} + \frac{\partial w}{\partial z} = 0$$

$$\frac{\partial c}{\partial t} + (\mathbf{u} \cdot \nabla) c + w \frac{\partial c}{\partial z} - \mathcal{C} = (\mathbf{u}^{st} \cdot \nabla) c - w^{st} \frac{\partial c}{\partial z} + \frac{\partial}{\partial z} \mathcal{E} \left[\frac{\partial c}{\partial z} \right]$$



Ocean dynamics and sediment

Bottom boundary layer

Bottom stress matters:

=> erosion and resuspension

=> bedload transport

Sediment :

=> change rugosity

Classical formulations :

$$\tau_{bx} = (\gamma_1 + \gamma_2 \sqrt{u^2 + v^2}) u$$

$$\tau_{by} = (\gamma_1 + \gamma_2 \sqrt{u^2 + v^2}) v$$

$$\tau_{bx} = \frac{\kappa^2}{\ln^2(z/z_0)} \sqrt{u^2 + v^2} u$$

$$\tau_{by} = \frac{\kappa^2}{\ln^2(z/z_0)} \sqrt{u^2 + v^2} v$$

=> BBL formulation :

- account for current stress at the bottom
- account for wave shear stress
- Sediment dependent z_0

$$\bar{\tau}_{wc} = \tau_c \left(1 + 1.2 \left(\frac{\tau_w}{\tau_w + \tau_c} \right)^{3.2} \right)$$

$$\tau_c = \frac{\kappa^2}{\ln^2(z/z_0)} |u|^2$$
$$\tau_w = 0.5 \rho f_w u_b^2$$

Models and features

Models and features

Sediment modeling : models

2 models available :

- USGS model : cpp key SEDIMENT
 - « legacy » model
 - originally included in ROMS-AGRIF
 - available in ROMS-RUTGERS and OAWST

- IFREMER model : cpp key MUSTANG
 - french model
 - originally included in MARS3D
 - available since 1.2 (just released)

Models and features

Sediment modeling : models and processes

- both model focus on non-cohesive sediment
- Same (main) processes for both
- Developments underway for cohesive processes
- In this presentation : USGS only
- but :
 - MUSTANG documented
 - Test cases with both models (Guillaume presentation)

Models and features

Sediment modeling : main processes in CROCO

- Transport in the water column
- Erosion / deposition
- Bedload transport
- Bed evolution (sand, mud, mixed)
- Morphological evolution

IMPLEMENTATION

EQUATIONS

Implementation

Transport

For each class of sediment :

$$\underbrace{\frac{\partial C}{\partial t}}_{\text{RATE}} = - \underbrace{\vec{\nabla} \cdot \vec{v} C}_{\text{ADVECTION}} + \underbrace{D_C}_{\text{MIXING}} - \underbrace{\frac{\partial w_s C}{\partial z}}_{\text{SETTLING}} + \underbrace{\frac{E}{\delta z_b} \Big|_{z=z_b}}_{\text{EROSION}}$$

C : sediment concentration
 \vec{v} : Lagrangian velocity

- multiple sediment classes :
grain size, density, settling velocity, erosion rate, bed porosity, and critical shear stress for erosion

- advection-diffusion (like T & S, bio etc)
- monotonic scheme (eventually)
- zero-flux boundary condition (diffusion)
- standard boundary conditions

Implementation

Deposition

$$\underbrace{\frac{\partial C}{\partial t}}_{\text{RATE}} = - \underbrace{\vec{\nabla} \cdot \vec{v} C}_{\text{ADVECTION}} + \underbrace{D_C}_{\text{MIXING}} - \underbrace{\frac{\partial w_s C}{\partial z}}_{\text{SETTLING}} - \underbrace{\frac{E}{\delta z_b} \Big|_{z=z_b}}_{\text{EROSION}}$$

=> settling velocity w_s

- sink term
- constant velocity (input parameter)
- class (size) dependent

Implementation

Erosion : non-cohesive case

$$\underbrace{\frac{\partial C}{\partial t}}_{\text{RATE}} = - \underbrace{\vec{\nabla} \cdot \vec{v} C}_{\text{ADVECTION}} + \underbrace{D_C}_{\text{MIXING}} - \underbrace{\frac{\partial w_s C}{\partial z}}_{\text{SETTLING}} + \underbrace{\frac{E}{\delta z_b} \Big|_{z=z_b}}_{\text{EROSION}}$$

- source term
- erosion flux (sea-floor only)
- class (size) dependent

$$E = E_0(1 - p) \phi \left(\frac{\tau_s}{\tau_c} - 1 \right) \text{ for } \tau_s > \tau_c$$

E_0 : erosion rate

p : porosity

ϕ : sediment fraction

τ_s : shear stress

τ_c : critical stress

Implementation

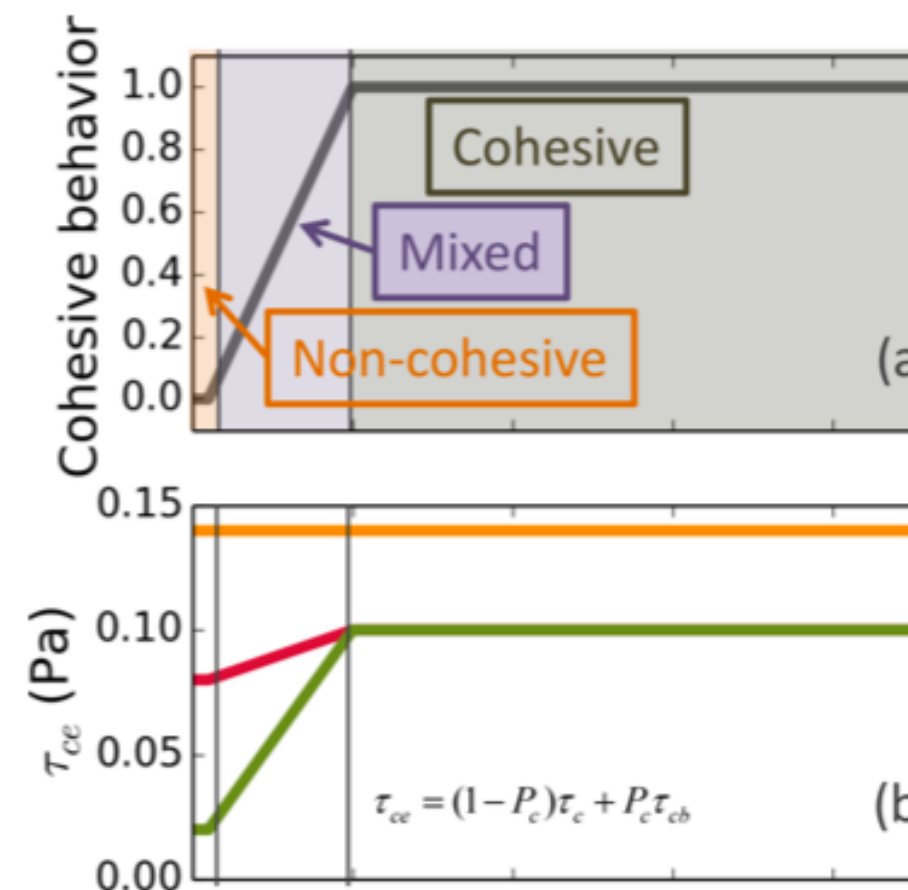
Erosion : mixed or cohesive case

$$\underbrace{\frac{\partial C}{\partial t}}_{\text{RATE}} = - \underbrace{\vec{\nabla} \cdot \vec{v} C}_{\text{ADVECTION}} + \underbrace{\mathcal{D} C}_{\text{MIXING}} - \underbrace{\frac{\partial w_s C}{\partial z}}_{\text{SETTLING}} + \underbrace{\frac{E}{\delta z_b} \Big|_{z=z_b}}_{\text{EROSION}}$$

$$E = E_0(1 - p) \phi \left(\frac{\tau_s}{\tau_c} - 1 \right) \text{ for } \tau_s > \tau_c$$

Time dependent critical stress τ_c :

- sediment classes => cohesive or not
- critical layer stress :
- erosion capacity depends on critical stress:
 - global property of the layer, not of the sediment classes
 - increases with depth
 - equilibrium profile updated at each time step
- effective instantaneous stress: damping to this equilibrium profile



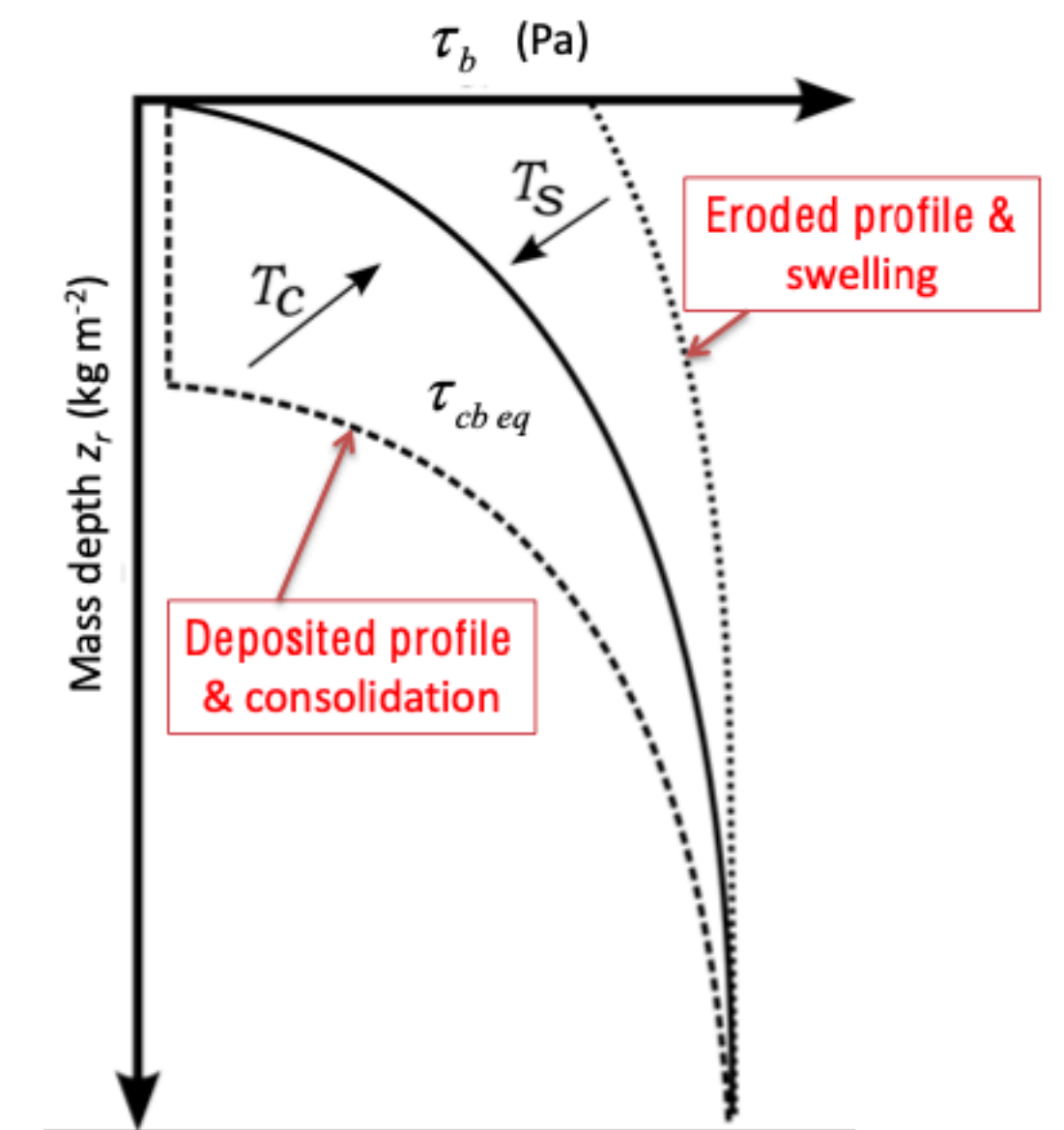
τ_c : critical stress

E_0 : erosion rate

p : porosity

ϕ : sediment fraction

τ_s : shear stress



$$\tau_{cb eq} = a \exp \left[\frac{\ln(z_p) - \text{offset}}{\text{slope}} \right]$$

Mixed case : $\tau_{ce} = \max [P_c \tau_{cb} + (1 - P_c) \tau_c, \tau_c]$

Implementation

Bedload

- not resolved explicitly
- bi-dimensional
- different parametrisations available (Φ : transport rate)

=> bedload flux

$$q_b = \Phi \sqrt{(s - 1)gd_{50}^3\rho_s}$$

=> slope effect

$$q_b \left(\frac{0.65}{(0.65 - \tan \beta) \cos \beta} \right)$$

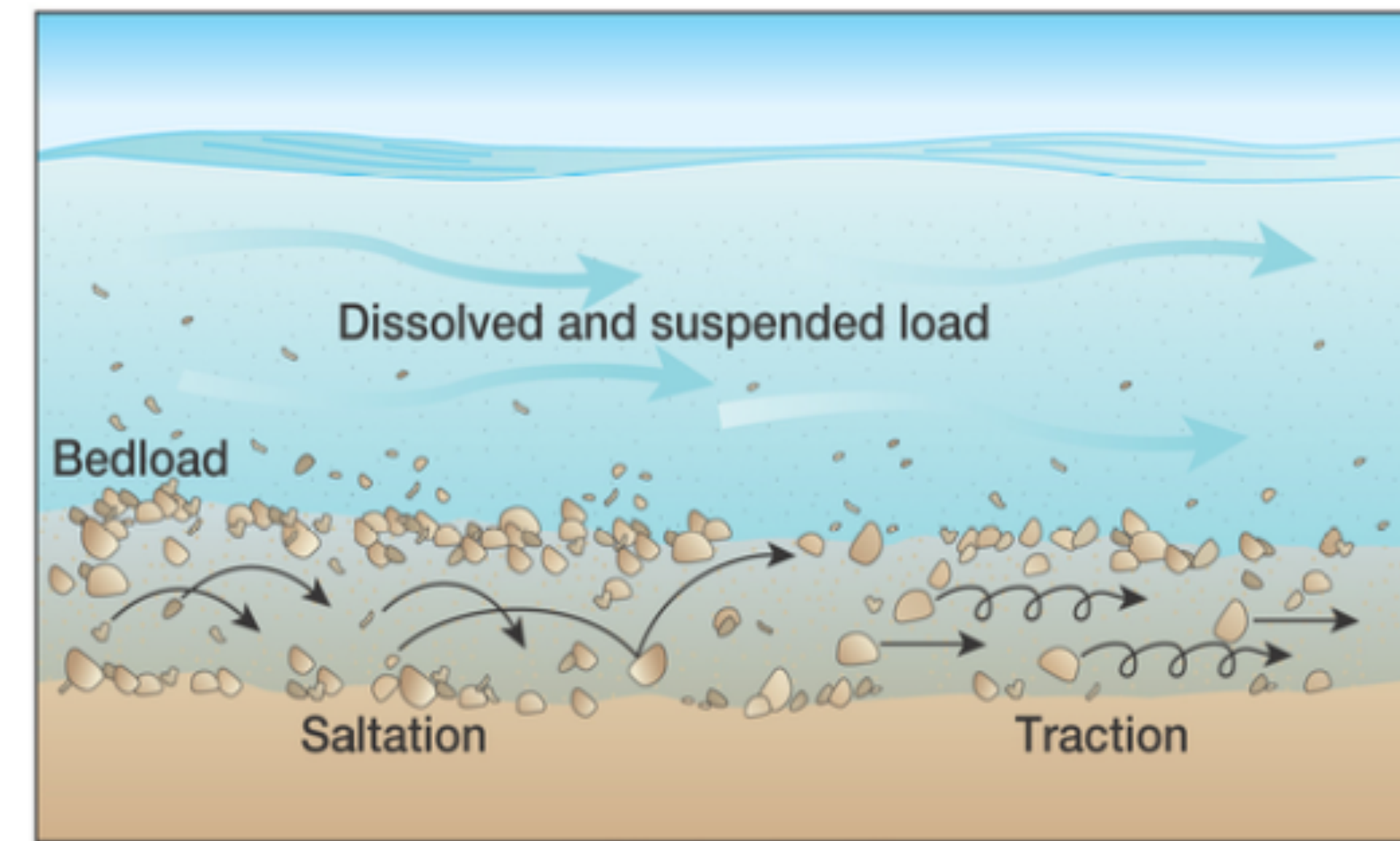
d_{50} : median size

ρ_s : grain density

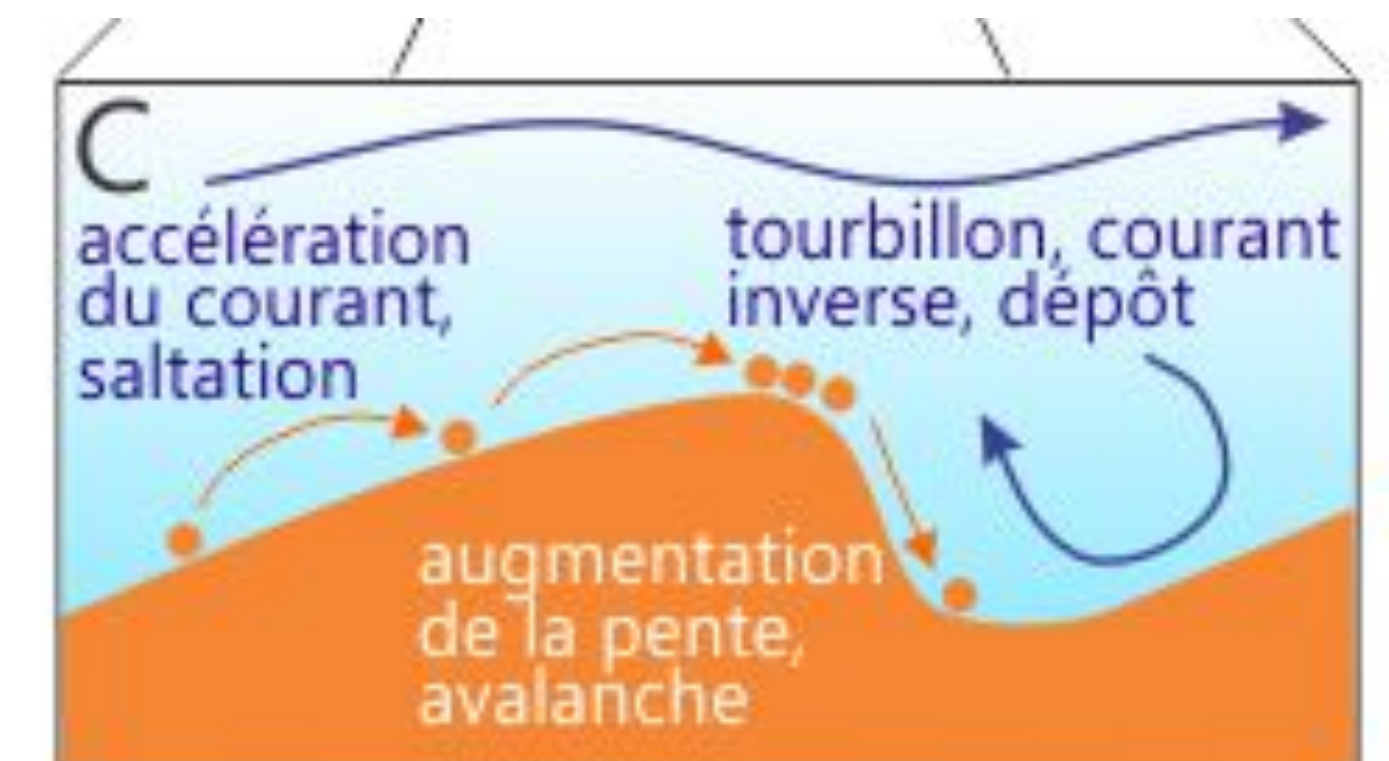
τ_c : critical stress

$$s = \rho/\rho_s$$

$$\beta = \tan^{-1}(dz_b/dx)$$



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Implementation

Bedload : Meyer-Peter Müller formulation

Case of rivers, continental shelves etc

Transport rate :

$$\Phi = \max [8(\theta_s - \theta_c)^{1.5}, 0]$$

Φ : transport rate (class dependent)

θ_s : Shield parameter

θ_c : critical Shield parameter

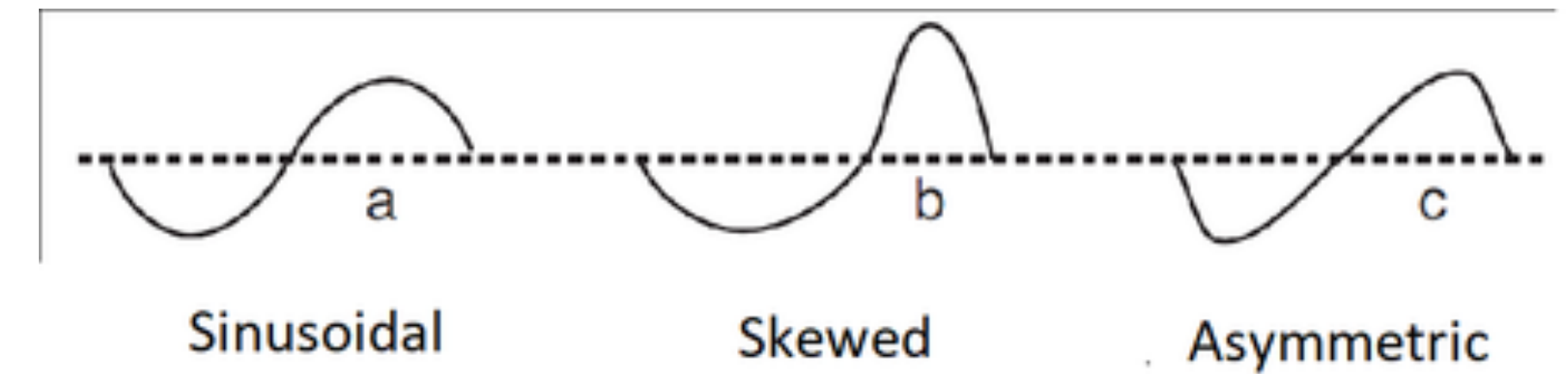
$$\theta_s = \frac{\tau_s}{(s - 1)gd_{50}}$$

τ_s : skin friction

$$\tau_s = \sqrt{\tau_{sx}^2 + \tau_{sy}^2}$$

Implementation

Bedload : Van der A formulation



Case of non-linear waves : asymmetric transport, lag effect ...

- compute asymmetry
- Shield parameter at Ralph cycle)
- Evaluate phase lag

=> Transport rate : crest + through

$$\Phi = \frac{1}{T} \left[\frac{\theta_c}{|\theta_c|^{1/2}} T_c \left(\Omega_{cc} + \frac{T_c}{2T_{cu}} \Omega_{tc} \right) + \frac{\theta_t}{|\theta_t|^{1/2}} T_t \left(\Omega_{tt} + \frac{T_t}{2T_{tu}} \Omega_{ct} \right) \right],$$

$$\Omega_i = \mathcal{F}(Shield Cr) = \max \left(11 (|\theta_i| - \theta_{cr})^{1.2}, 0 \right),$$

Implementation

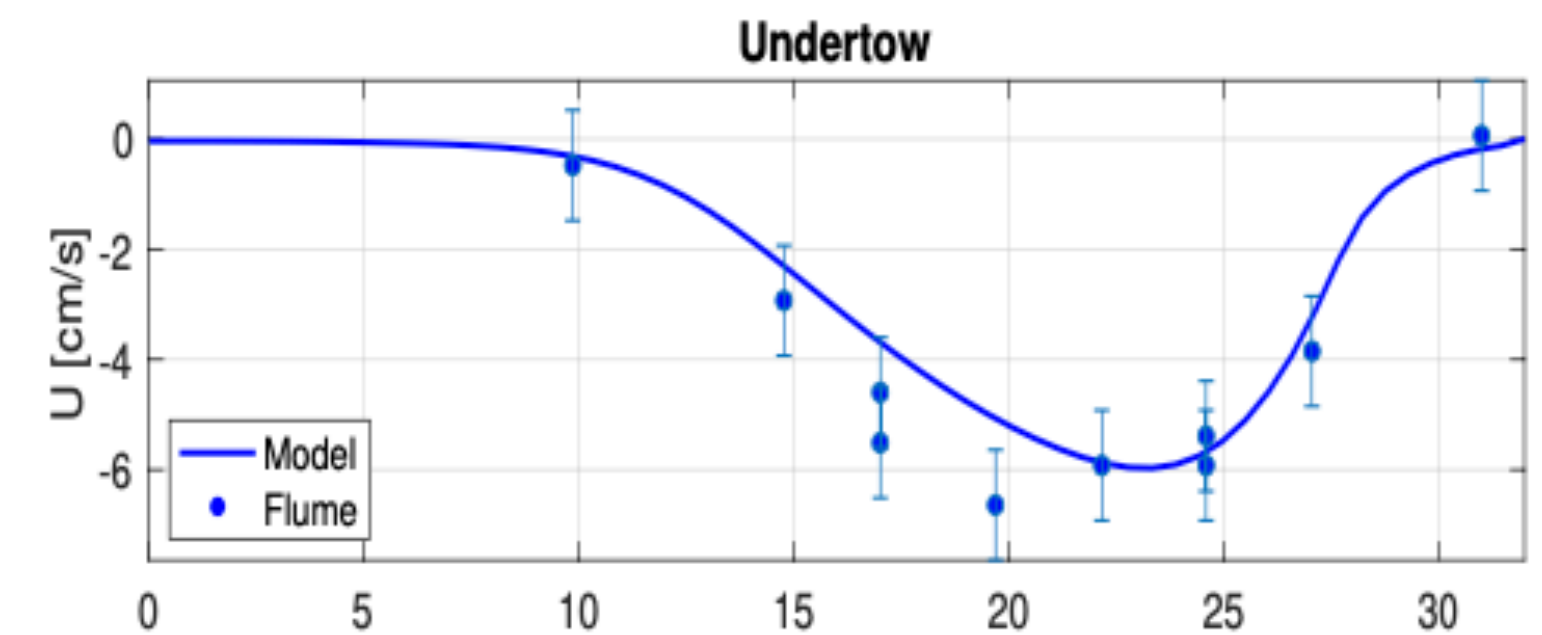
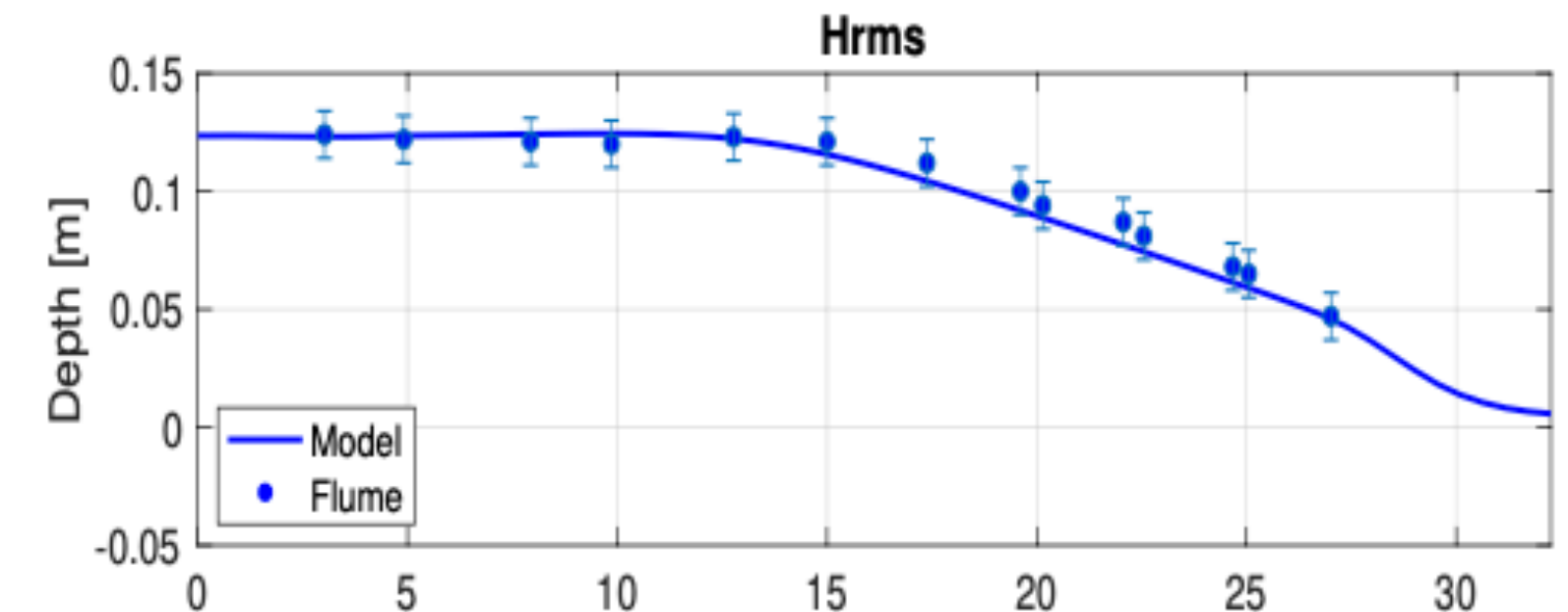
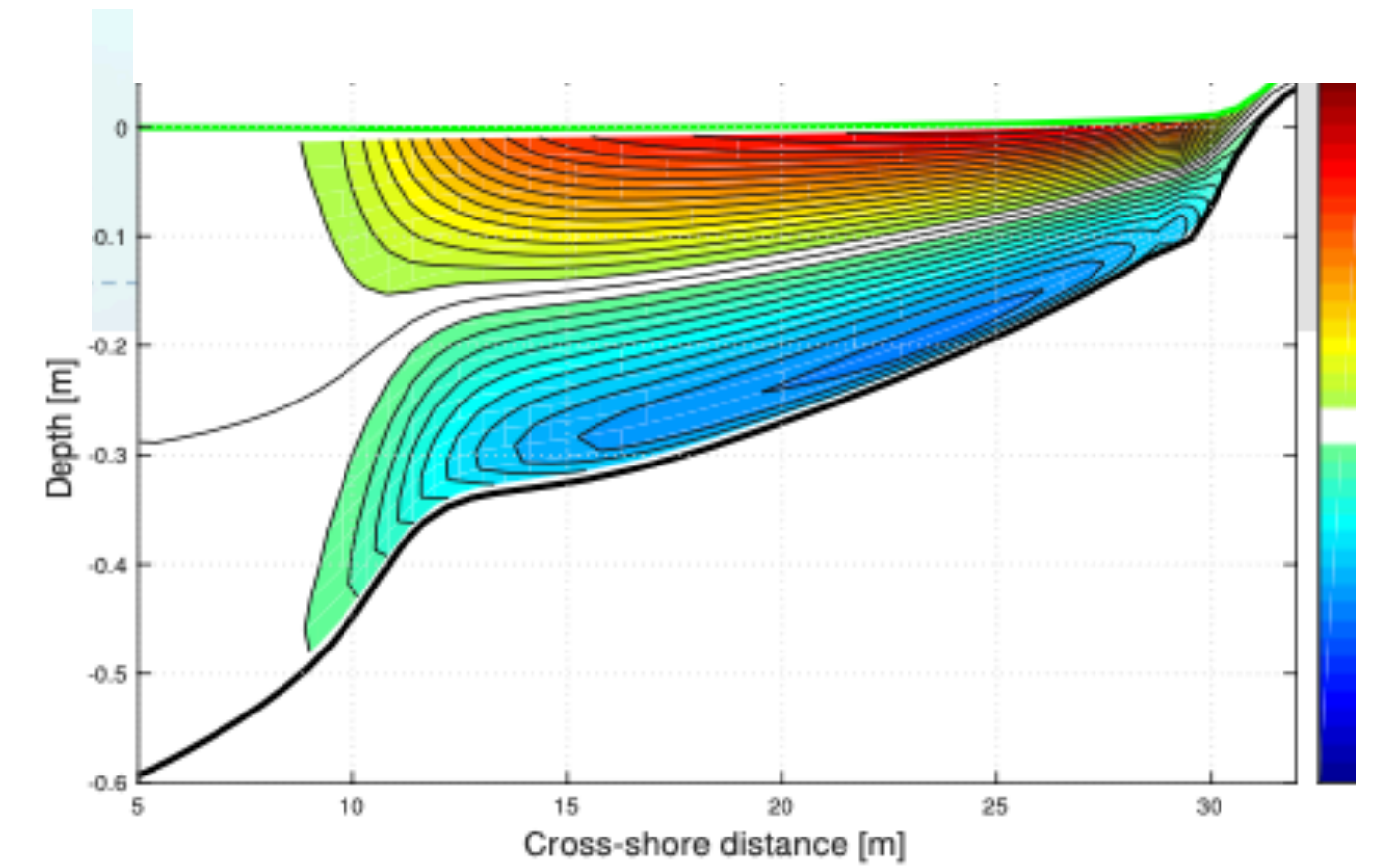
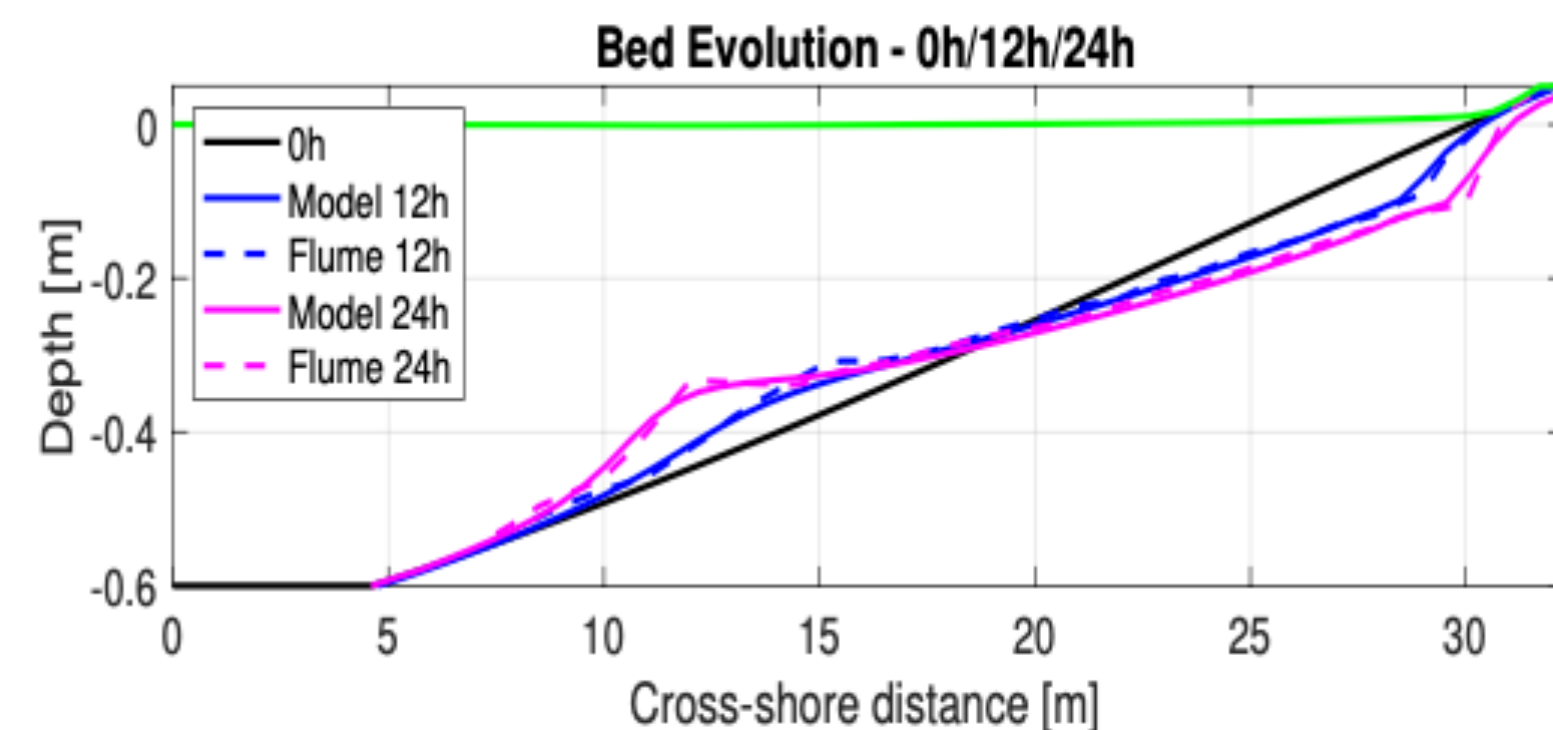
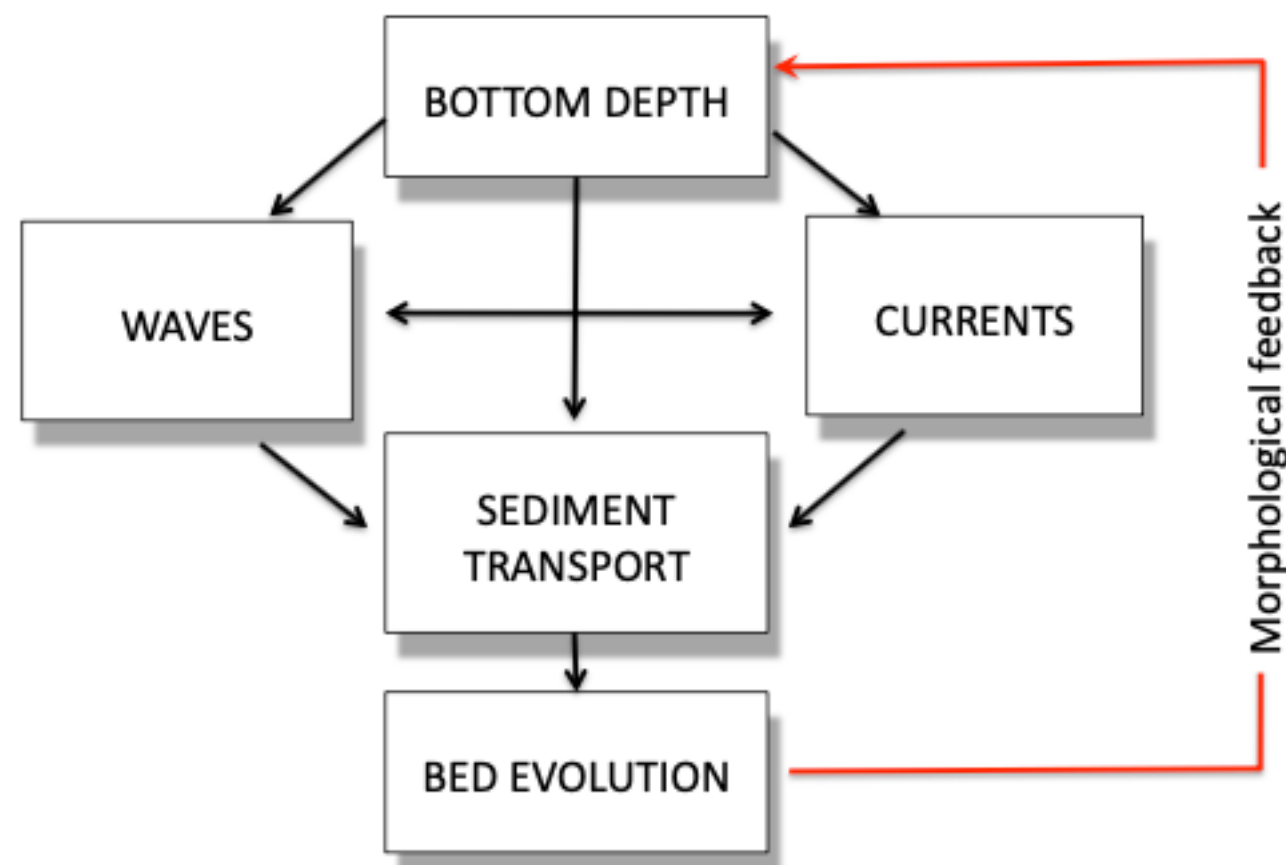
Morphodynamics

Exner equation : divergence of sediment fluxes

i.e. difference between erosion and deposition
+ bedload fluxe

$$\frac{\partial z_b}{\partial t} = -\frac{f_{mor}}{1-p} \left(\frac{\partial q_b}{\partial x} - w_s \frac{\partial C}{\partial z} + E \right).$$

- modification of vertical velocity
- speed-up equilibration

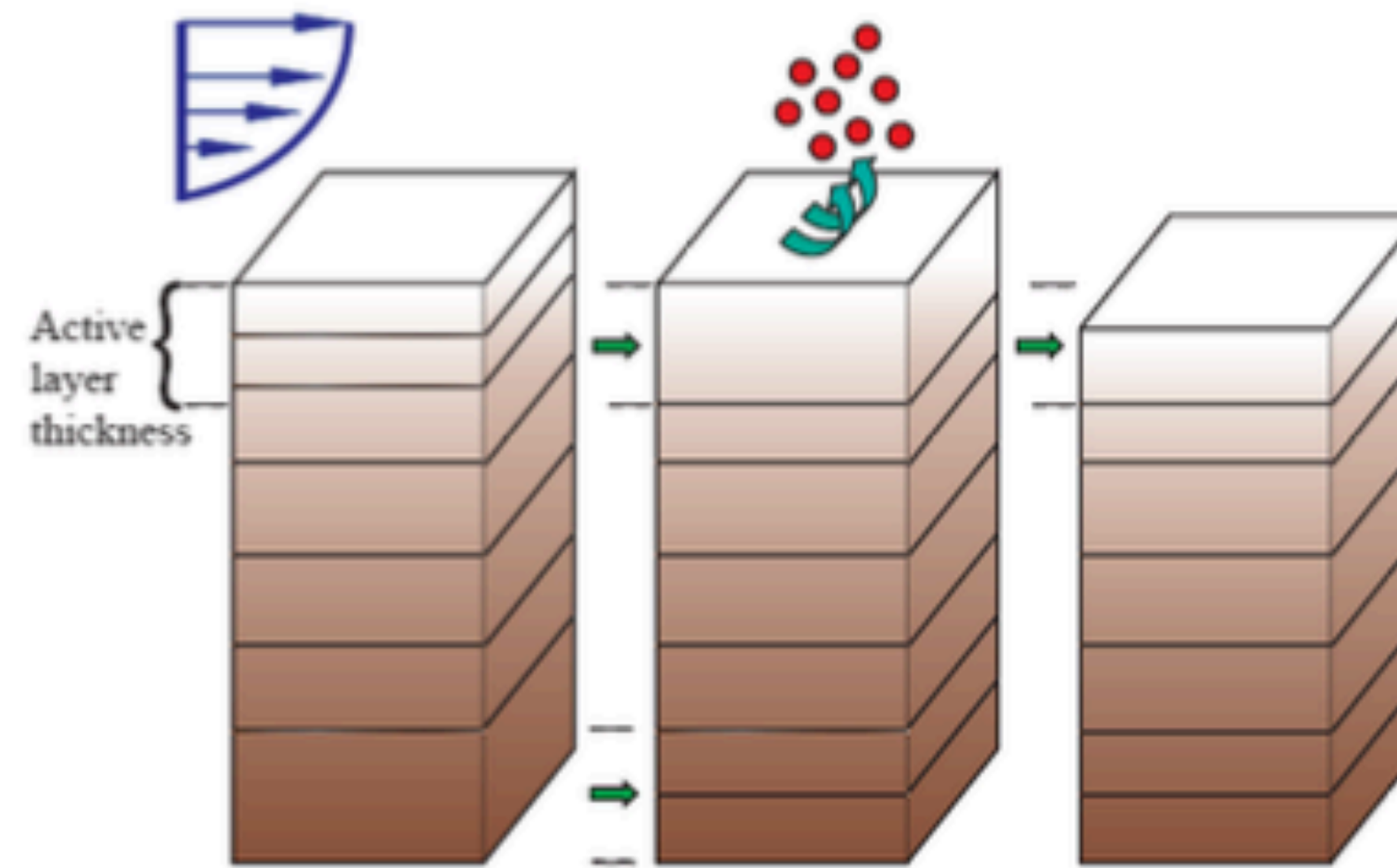


Implementation

Bed model

Active layer thickness (Harris and Wiberg, 1997).

$$Z_a = k_1(\tau_w - \tau_c) + k_2 D_{50}$$

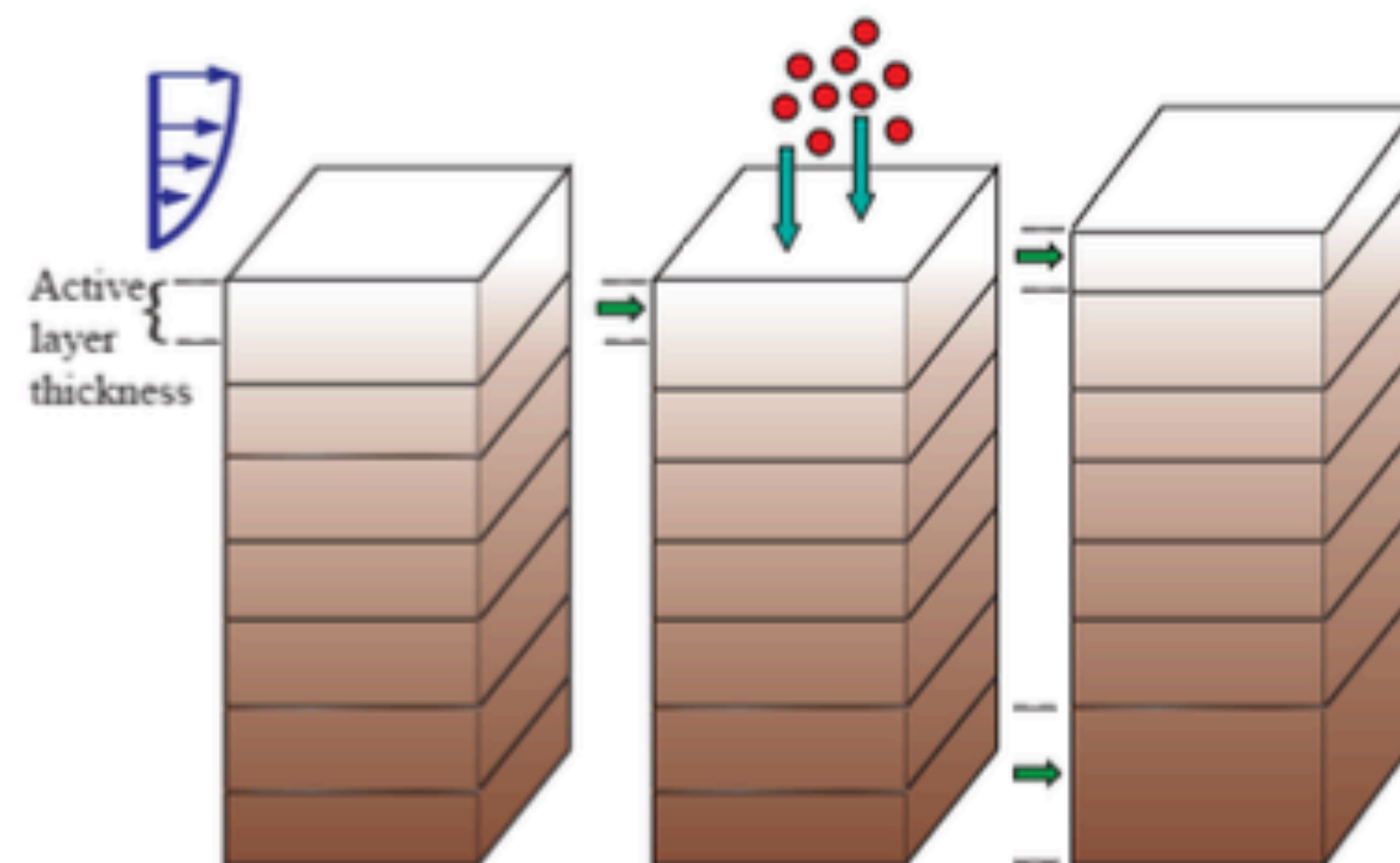


Erosion. ($\tau_b > \tau_c$)

Mix sediment from lower layers so that surface layer is at least z_a thick. Split bottom layer. Erode from surface layer.

erosion_flux_i =

$$\text{MIN} \left[\begin{array}{l} dt * E_i * (1 - \text{poro}) * \text{frac}_i * (\tau_w / \tau_{c,i} - 1) \\ \rho_i * (1 - \text{poro}) * \text{frac}_i * z_a + \text{dep_flux}_i \end{array} \right]$$



Deposition.

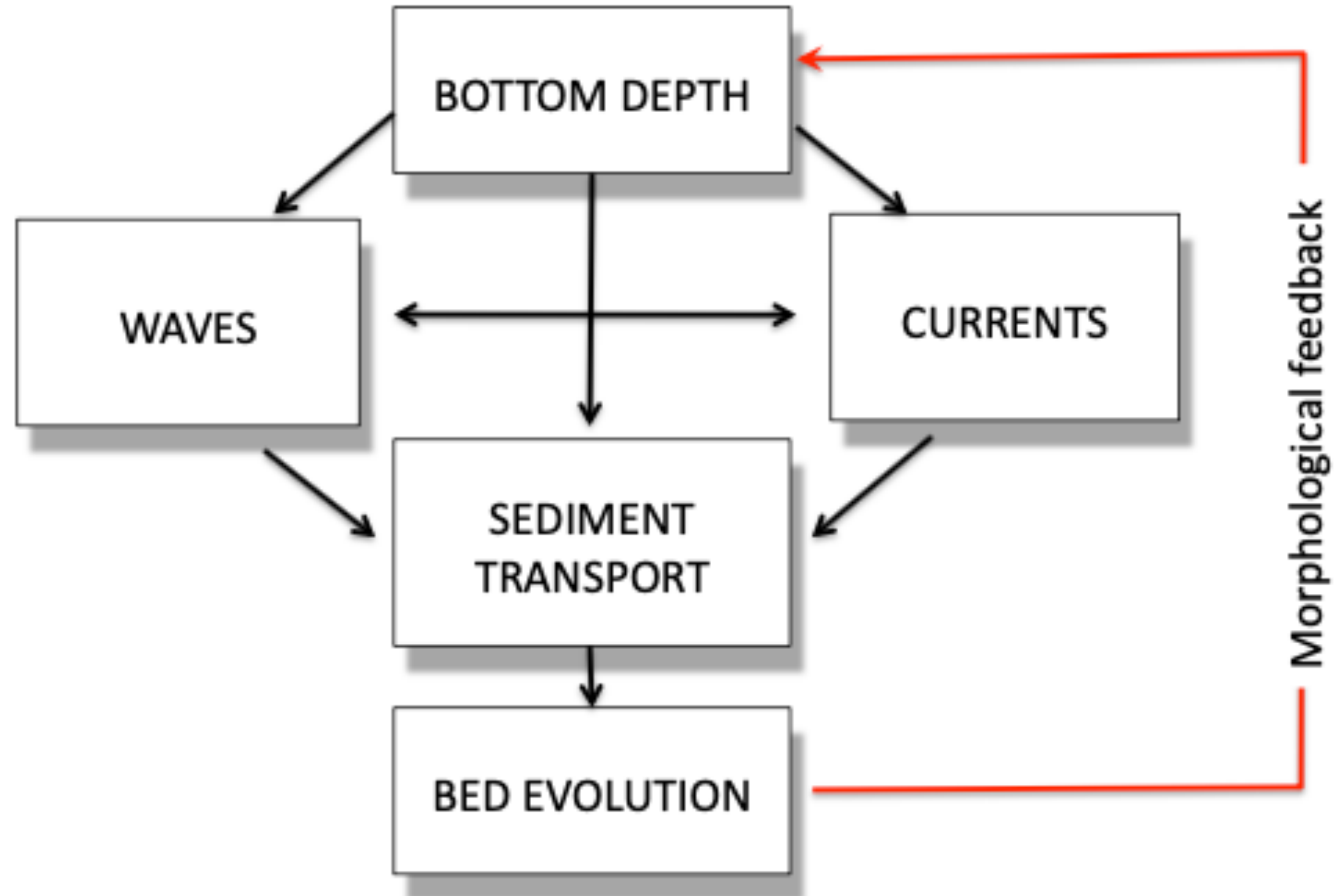
Rule: create new layer if deposition > 5 mm (user defined). Mix surface layer to be at least z_a thick. Combine bottom layer.

$$\frac{\partial C_i}{\partial t} = -w_{s,i} \frac{\partial C}{\partial z}$$

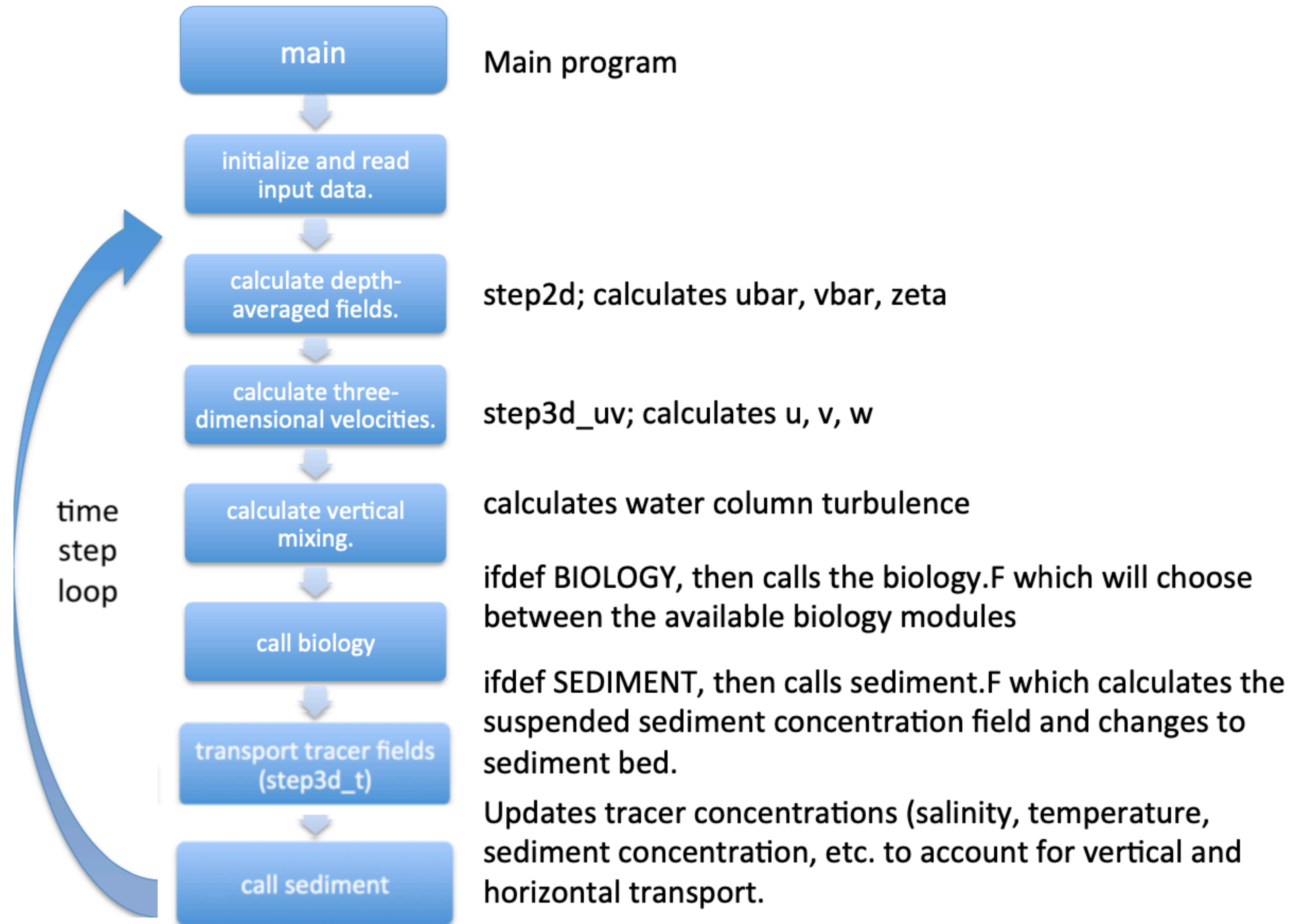
IMPLEMENTATION

CODE STRUCTURE

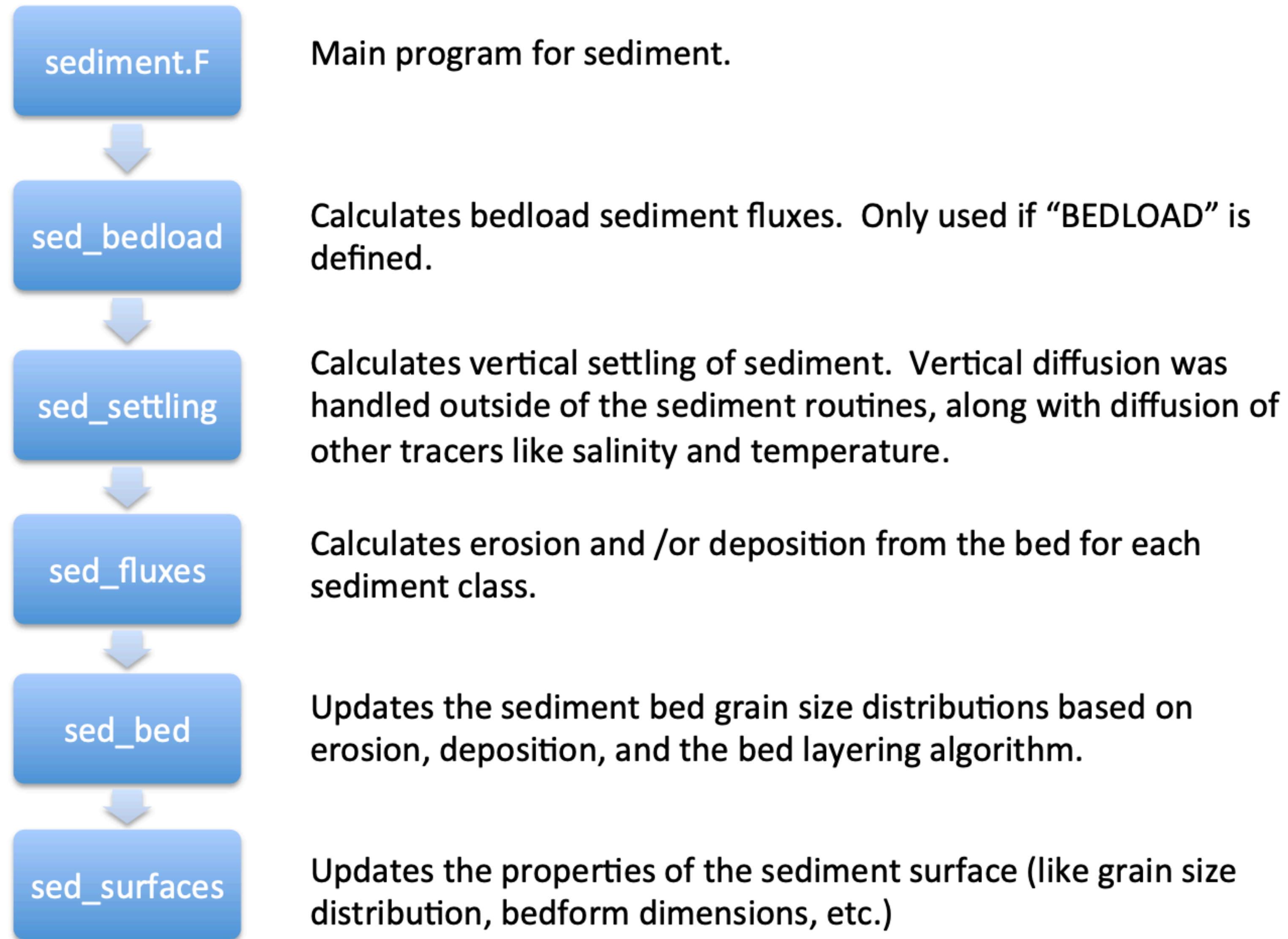
Code structure (1)



Code structure (2)



Code structure (3)



Code structure (4)

```
if defined NONLINEAR && defined SEDIMENT && defined BEDLOAD
```

This routine computes sediment bedload transport using the Meyer-Peter and Muller (1948) formulation for unidirectional flow and Soulsby and Damgaard (2005) algorithm that accounts for combined effect of currents and waves.

References:

Meyer-Peter, E. and R. Muller, 1948: Formulas for bedload transport
In: Report on the 2nd Meeting International Association Hydraulic
Research, Stockholm, Sweden, pp 39-64.

Soulsby, R.L. and J.S. Damgaard, 2005: Bedload sediment transport
in coastal waters, Coastal Engineering, 52 (8), 673-689.

Warner, J.C., C.R. Sherwood, R.P. Signell, C.K. Harris, and H.G.
Arango, 2008: Development of a three-dimensional, regional,
coupled wave, current, and sediment-transport model, Computers
& Geosciences, 34, 1284-1306.

sed_bedload

1. Calculate correct bed stresses.
2. Calculate bedload transport rate using one of two relationships.
3. Accounts for bed slope.
4. Calculate bedload flux convergence and divergence that lead to erosion and deposition.
5. Limit erosion to amount of sediment available, and deposition to not shoaling.
6. Updates sediment bed properties.

Code structure (5)

```
#if defined NONLINEAR && defined SEDIMENT && defined SUSPLOAD
```

```
! ----- !  
! This routine computes the vertical settling (sinking) of suspended !  
! sediment via a semi-Lagrangian advective flux algorithm. It uses a !  
! parabolic, vertical reconstruction of the suspended sediment in !  
! the water column with PPT/WENO constraints to avoid oscillations. !
```

```
! References: !
```

```
! Colella, P. and P. Woodward, 1984: The piecewise parabolic method !  
! (PPM) for gas-dynamical simulations, J. Comp. Phys., 54, 174-201. !
```

```
! Liu, X.D., S. Osher, and T. Chan, 1994: Weighted essentially !  
! nonoscillatory schemes, J. Comp. Phys., 115, 200-212. !
```

```
! Warner, J.C., C.R. Sherwood, R.P. Signell, C.K. Harris, and H.G. !  
! Arango, 2008: Development of a three-dimensional, regional, !  
! coupled wave, current, and sediment-transport model, Computers !  
! & Geosciences, 34, 1284-1306. !
```

sed_settling

1. Vertical settling of sediment.
2. Biology routine uses same scheme for particulate classes.
3. Updates concentration fields for vertical settling.
4. Also calculates flux of sediment into the bed.
5. Does the calculations separately for each sediment type.

Code structure (6)

```
#if defined NONLINEAR && defined SEDIMENT && defined SUSPLOAD  
  
-----  
This computes sediment bed and water column exchanges: deposition,  
resuspension, and erosion.  
  
References:  
  
Warner, J.C., C.R. Sherwood, R.P. Signell, C.K. Harris, and H.G.  
Arango, 2008: Development of a three-dimensional, regional,  
coupled wave, current, and sediment-transport model, Computers  
& Geosciences, 34, 1284-1306.  
-----
```

sed_fluxes

1. Exchange of sediment between water column and seabed.
2. First – calculates bed stresses.
3. Calculates erosion based on

$$E_{s,m} = E_{0,m}(1 - \phi) \frac{\tau_{sf} - \tau_{ce,m}}{\tau_{ce,m}}, \quad \text{when } \tau_{sf} > \tau_{ce,m} \quad (23)$$

where E_s is the surface erosion mass flux ($\text{kg m}^{-2} \text{s}^{-1}$), E_0 is a bed erodibility constant ($\text{kg m}^{-2} \text{s}^{-1}$), ϕ is the porosity (volume of voids/total volume) of the top bed layer, and m is an index

4. Erosion limited to amount of each size class in the surface layer + whatever would have settled.
5. The net erosion for each sediment class is called “ero_flux”.
6. Updates water column concentration in bottom water layer for the erosion and deposition.

Code structure (7)

sed_bed

1. The longest sediment routine (800 lines).
2. Keeps track of sediment distributions and properties in bed layers.
3. Has net erosion for each sediment class as “ero_flux” from sed_fluxes.F.
4. Has amount settling to bed as “settling_flux” from sed_settling.F.
5. The net erosion for each sediment class is the difference of “ero_flux” and “settling_flux”.
 - a. If “ero_flux – settling_flux” < 0, then you have net deposition of this sediment class. Add sediment to the top layer. When the top layer gets thick, split off a new top layer.
 - b. If “ero_flux – settling_flux” > 0, then you have net erosion of this sediment class. Remove sediment from the top layers.
 - c. Adjust layers if you needed to add a complete layer or erode one.

```
#if defined NONLINEAR && defined SEDIMENT && !defined COHESIVE_BED
```

```
=====
```

```
This routine computes sediment bed layer stratigraphy.      !
```

```
Warner, J.C., C.R. Sherwood, R.P. Signell, C.K. Harris, and H.G. !  
Arango, 2008: Development of a three-dimensional, regional, !  
coupled wave, current, and sediment-transport model, Computers !  
& Geosciences, 34, 1284-1306. !
```

```
=====
```

IMPLEMENTATION

MODEL OPTIONS

Model options

BBL

Related CPP options:

BBL	Activate bottom boundary layer parametrization
ANA_WWAVE	Set analytical (constant) wave forcing (hs, Tp, Dir).
ANA_BSEDIM	Set analytical bed parameters (if SEDIMENT is undefined)
Z0_BL	Compute bedload roughness for ripple predictor and sediment purposes
Z0_RIP	Determine bedform roughness ripple height and ripple length for sandy bed
Z0_BIO	Determine (biogenic) bedform roughness ripple height and ripple length for silty beds

Preselected options:

```
#ifdef BBL
# ifdef OW_COUPLING
# elif defined WAVE_OFFLINE
# elif defined WKB_WWAVE
# else
# define ANA_WWAVE
# endif
# ifdef SEDIMENT
# undef ANA_BSEDIM
# else
# define ANA_BSEDIM
# endif
# ifdef SEDIMENT
# define Z0_BL
# else
# undef Z0_BL
# endif
# ifdef Z0_BL
# define Z0_RIP
# endif
# undef Z0_BIO
#endif
```

Model options

Sediment parameters

- Hard coded
 - Number of layers
 - Number of sediment classes

=> in param.h

```
!  
# ifdef SEDIMENT  
! NSAND      Number of sand classes  
! NMUD      Number of mud classes  
! NGRAV     Number of gravel classes (not implemented...)  
! NST       Number of sediment (tracer) size classes  
! NLAY      Number of layers in sediment bed  
!  
    integer NSAND, NMUD, NGRAV, NST, NLAY  
# ifdef DUNE  
#   ifdef ANA_DUNE  
        parameter (NSAND=1, NMUD=0, NGRAV=0)  
        parameter (NLAY=11)  
#   else  
        parameter (NSAND=2, NMUD=0, NGRAV=0)  
        parameter (NLAY=10)  
#   endif  
# elif defined SED_TOY  
#   if defined SED_TOY_RESUSP || defined SED_TOY_CONSOLID  
        parameter (NSAND=2, NMUD=2, NGRAV=0)  
        parameter (NLAY=41)  
#   elif defined SED_TOY_FLOC  
        parameter (NSAND=4, NMUD=15, NGRAV=0)  
        parameter (NLAY=20)  
#   elif defined SED_TOY_ROUSE  
        parameter (NSAND=0, NMUD=6, NGRAV=0)  
        parameter (NLAY=1)  
#   endif  
#   else  
        parameter (NSAND=2, NMUD=0, NGRAV=0)  
        parameter (NLAY=1)  
#   endif  
        parameter (NST=NSAND+NMUD+NGRAV)  
        parameter (ntrc_sed=NST)  
# else  
        parameter (ntrc_sed=0)  
# endif /* SEDIMENT */  
!
```


Model options

Sediment CPP keys

- Main keys :
 - SEDIMENT or MUSTANG
 - SUSPLOAD
 - BEDLOAD
- => stick with default choices

Related CPP options:

SUSPLOAD	Activate suspended load transport
BEDLOAD	Activate bedload transport
MORPHODYN	Activate morphodynamics
BEDLOAD_VANDERA	van der A formulation for bedload (van der A et al., 2013)
BEDLOAD_MPM	Meyer-Peter-Muller formulation for bedload (Meyer-Peter and Muller, 1948)
SLOPE_LESSER	Lesser formulation for avalanching (Lesser et al, 2004)
SLOPE_NEMETH	Nemeth formulation for avalanching (Nemeth et al, 2006)
BEDLOAD_UP1	Bedload flux interpolation: upwind 1rst order
BEDLOAD_UP5	Bedload flux interpolation: upwind 5th order
BEDLOAD_WENO5	Bedload flux interpolation: WENO 5th order
ANA_SEDIMENT	Set analytical sediment size, initial ripple and bed parameters
ANA_BPFLUX	Set kinematic bottom flux of sediment tracer (if different from 0)
SPONGE_SED	Gradually reduce erosion/deposition near open boundaries

Preselected options:

```
#ifdef SEDIMENT
# undef MUSTANG
# define ANA_SEDIMENT
# define SPONGE_SED
# define Z0_BL
# define Z0_RIP
# ifdef BEDLOAD
#   ifdef BEDLOAD_VANDERA /* default BEDLOAD scheme */
#   elif defined BEDLOAD_MPM
#   elif defined BEDLOAD_WULIN
#   elif defined BEDLOAD_MARIEU
#   else
#     if (defined WAVE_OFFLINE || defined WKB_WWAVE ||
        defined ANA_WWAVE || defined OW_COUPLING)
#       define BEDLOAD_VANDERA
#     else
#       define BEDLOAD_MPM
#     endif
#   endif
# endif
```

Model options

Input file

- Additional file at run time : sediment.in

Consistent with :

- Number of layers
- Number of sediment classes

```
1 Stitle (a80)
CROCO - Sediment - Test

2 Sd(1-NST), CSED, SRHO, WSED, ERATE, TAU_CE, TAU_CD, BED_FRAC(1:NLAY)
   0.125  9.9  2650.  9.4  25.0e-5  0.05  0.14  0.4  0.4
   0.050  0.0  2650.  1.6  4.0e-5  0.01  0.14  0.6  0.6

3 BTHK(1:NLAY)
   1.  10.

4 BPOR(1:NLAY)
   0.41  0.42

5 Hrip
   0.03

6 Lrip
   0.14

7 bedload_coeff
   0.

8 morph_fac
   10.

99 END of sediment input data
```

> **Sd** : Diameter of grain size class [mm].

> **CSED** : Initial concentration (spatially uniform) [kg/m3].

> **SRHO** : Density of sediment material of size class [kg/m3].

Quartz: SRHO=2650 kg/m³

> **WSED** : Settling velocity of size class [mm/s].

Typically (Soulsby, 1997):

$$WSED = 10^3 (visc (\sqrt{10.36^2 + 1.049D^3} - 10.36) / D_{50} \text{ [mm/s]})$$

with $D = D_{50} (g (SRHO/\rho_0 - 1) / (visc^2))^{0.33333}$

$$D_{50} = 10^{-3} Sd \text{ [m]}$$

$$visc = 1.3 \cdot 10^{-3} / \rho_0 \text{ [m}^2/\text{s]}$$

> **ERATE** : Erosion rate of size class [kg/m2/s].

Typically:

$$ERATE = 10^{-3} \gamma_0 WSED SRHO \text{ [kg/m}^2/\text{s]}$$

with $\gamma_0 = 10^{-3} - 10^{-5}$ (Smith & McLean, 1977)

> **TAU_CE** : Critical shear stress for sediment motion [N/m2]

(initiation of bedload for coarses, suspension for fines). Typically : $TAU_{CE} = 6.4 \cdot 10^{-7} \rho_0 WSED^2$ [N/m2]

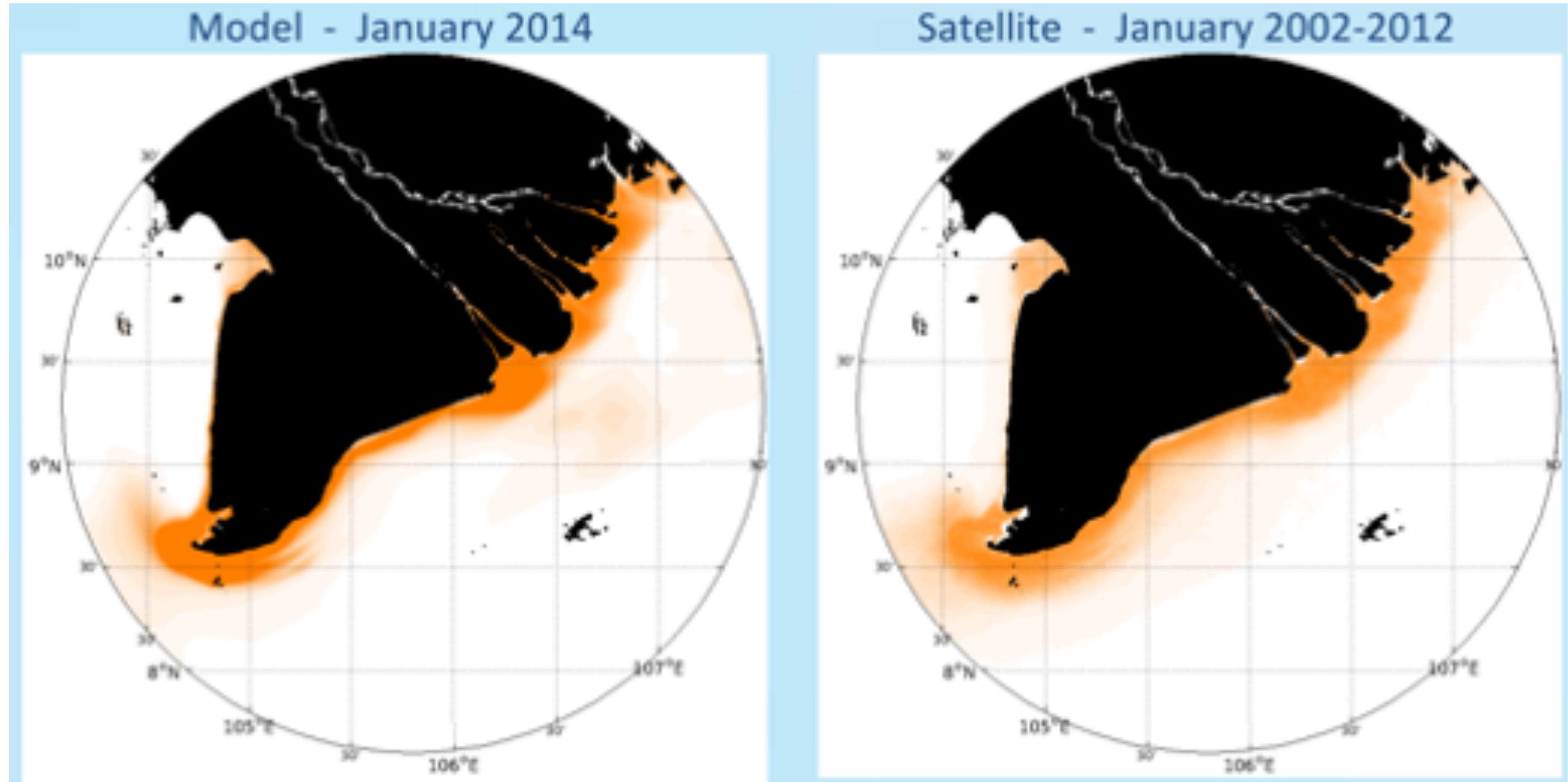
> **TAU_CD** : Critical shear stress for deposition of cohesive sediments [N/m2]

> **BED_FRAC** : Volume fraction of each size class in each bed layer (NLAY columns)

$$[0 < BED_FRAC < 1]$$

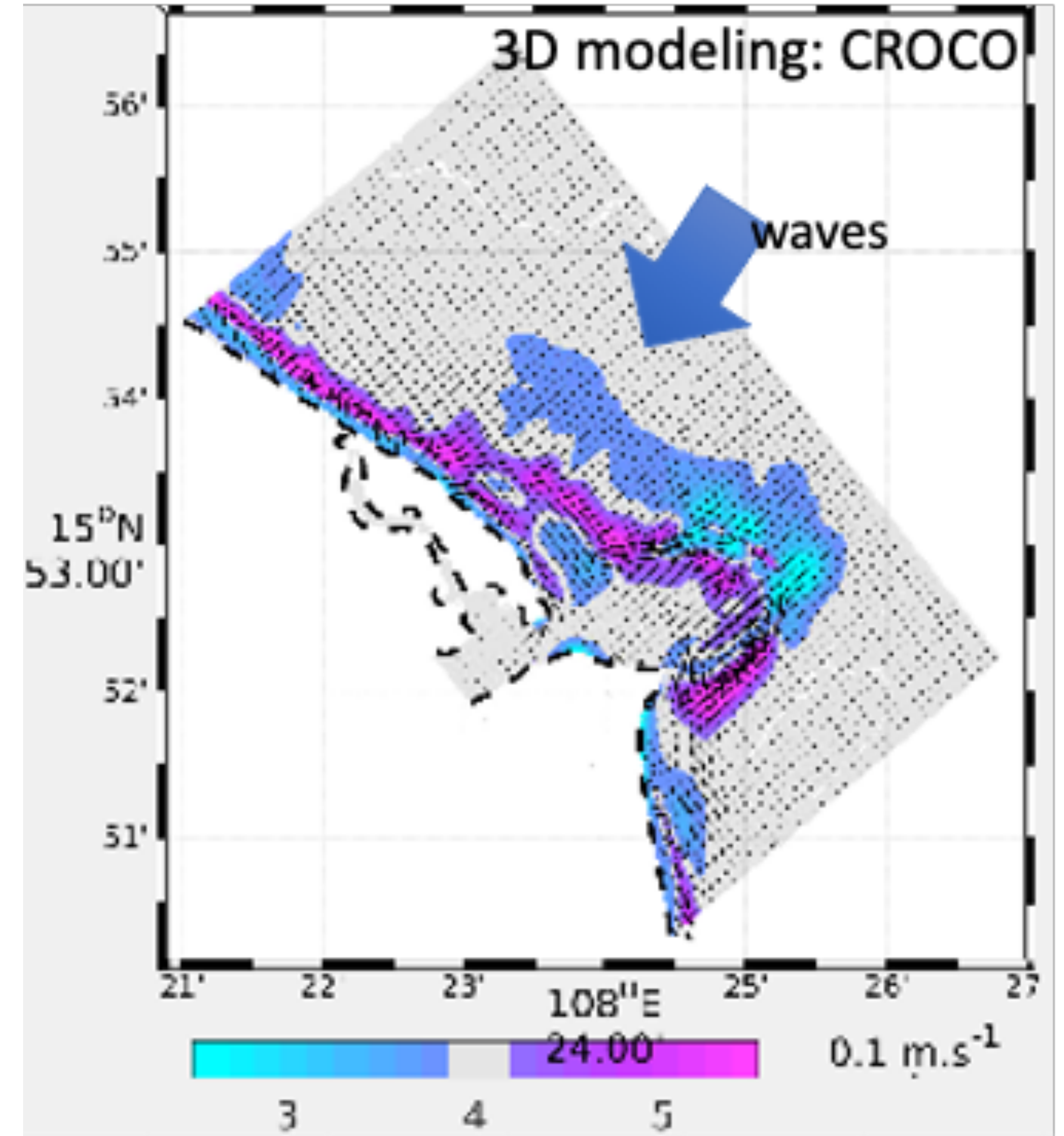
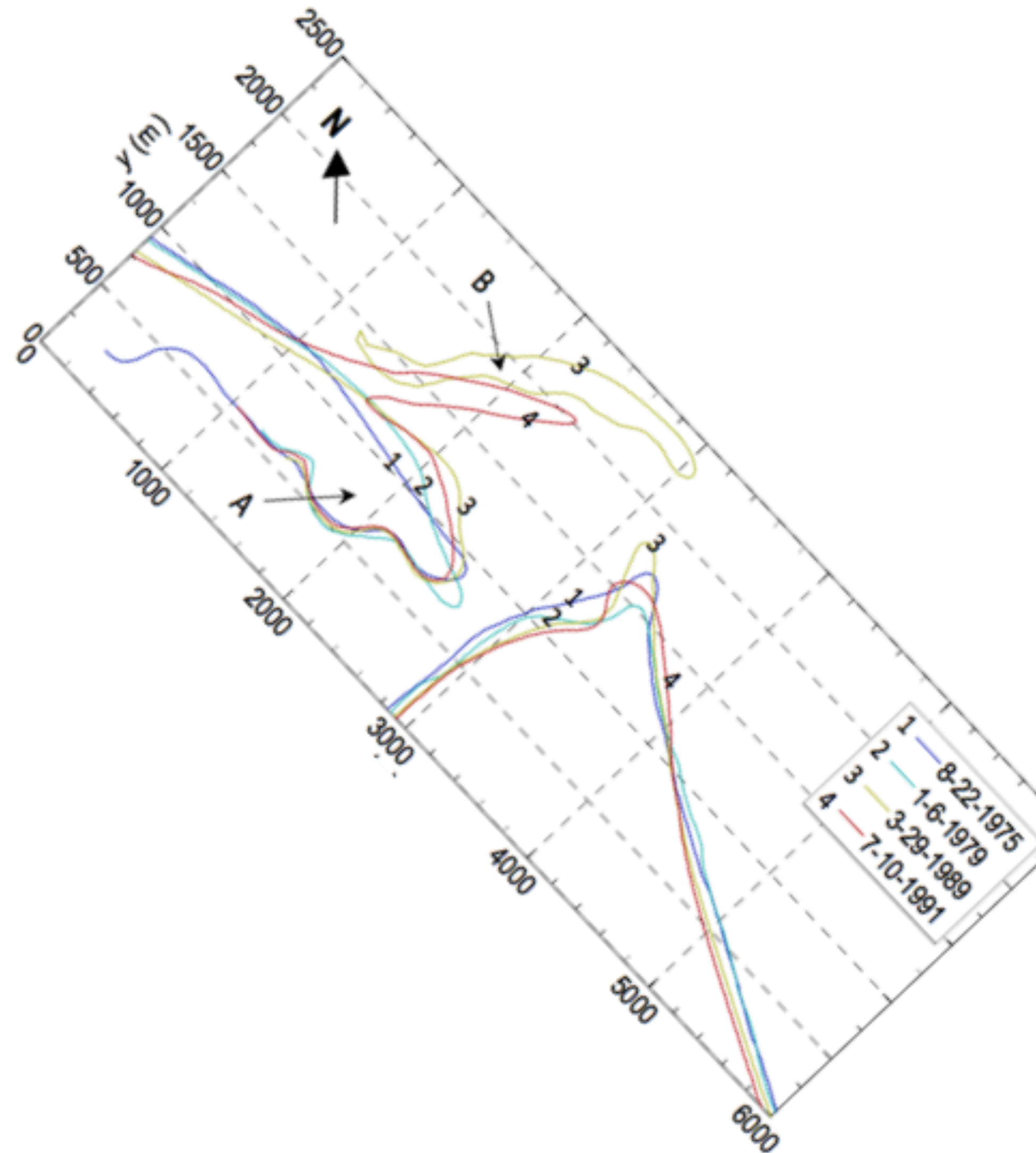
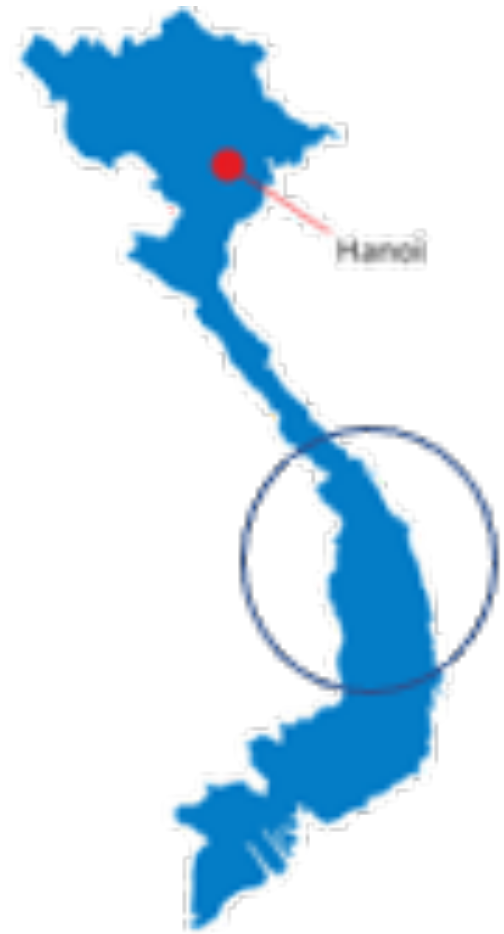
EXAMPLES

EXAMPLE 1



Gratiot et al., 2017, Ha et al., 2018, Marchesiello et al., 2019

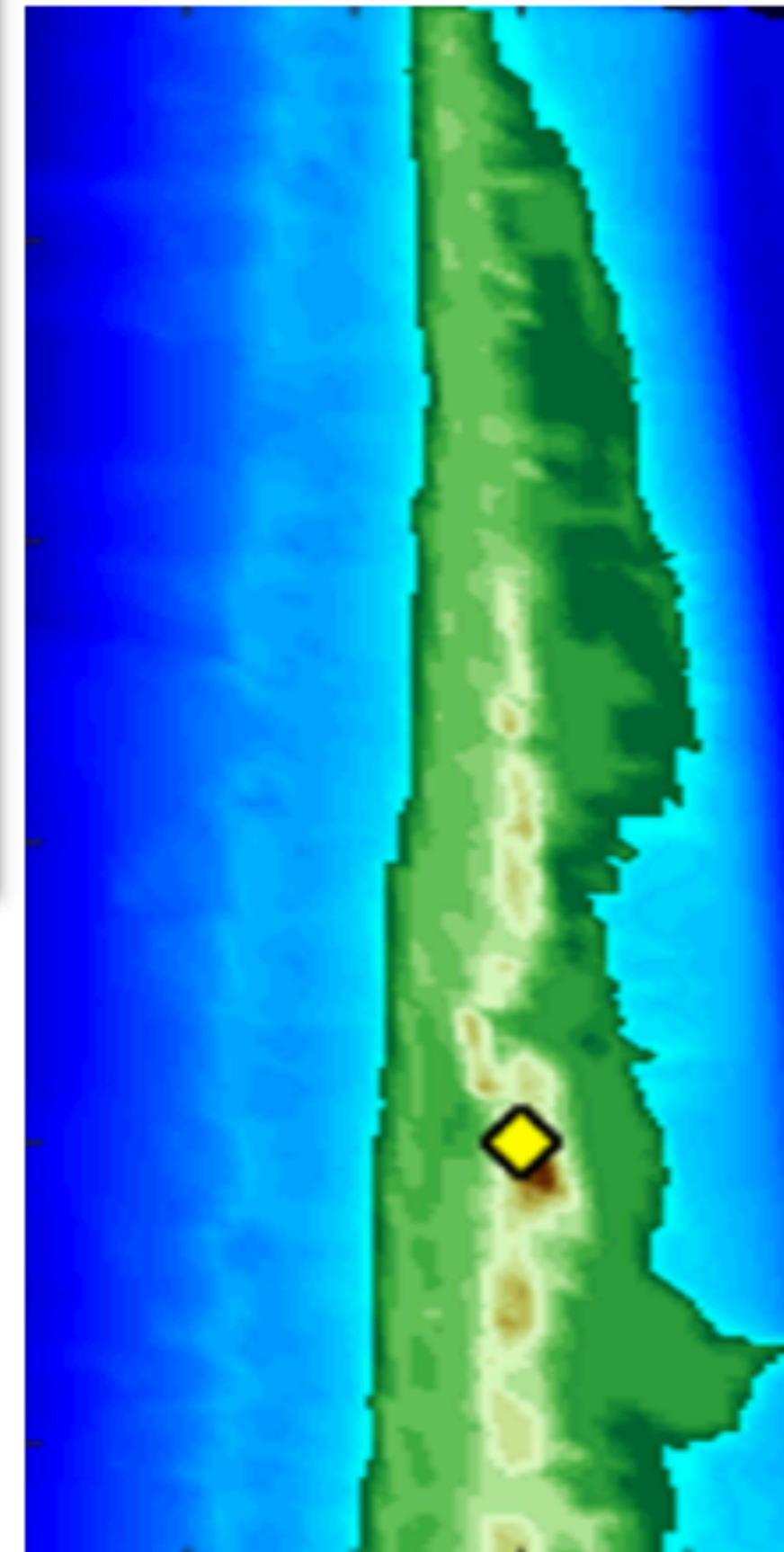
EXAMPLE 2



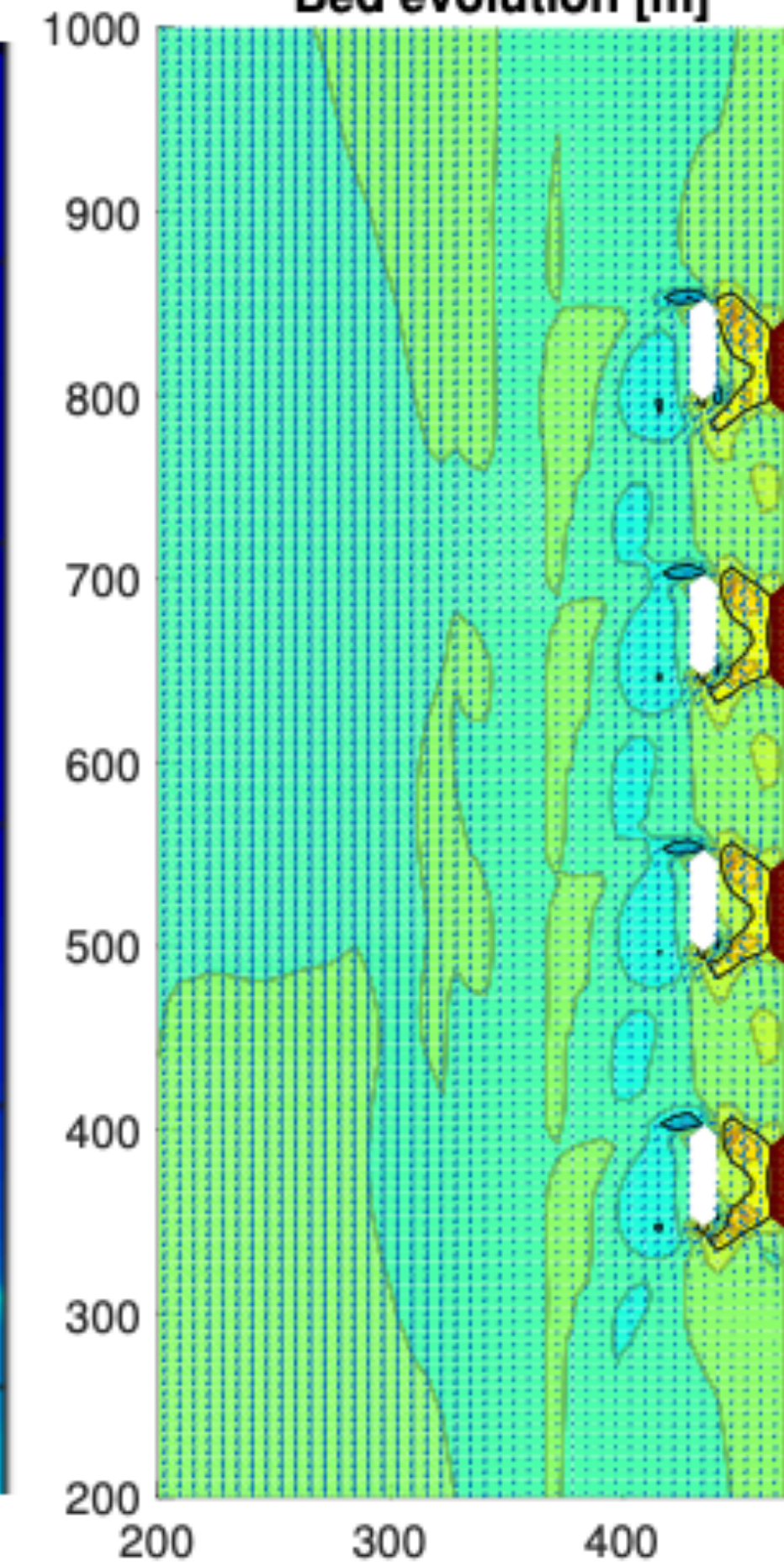
EXAMPLE 3



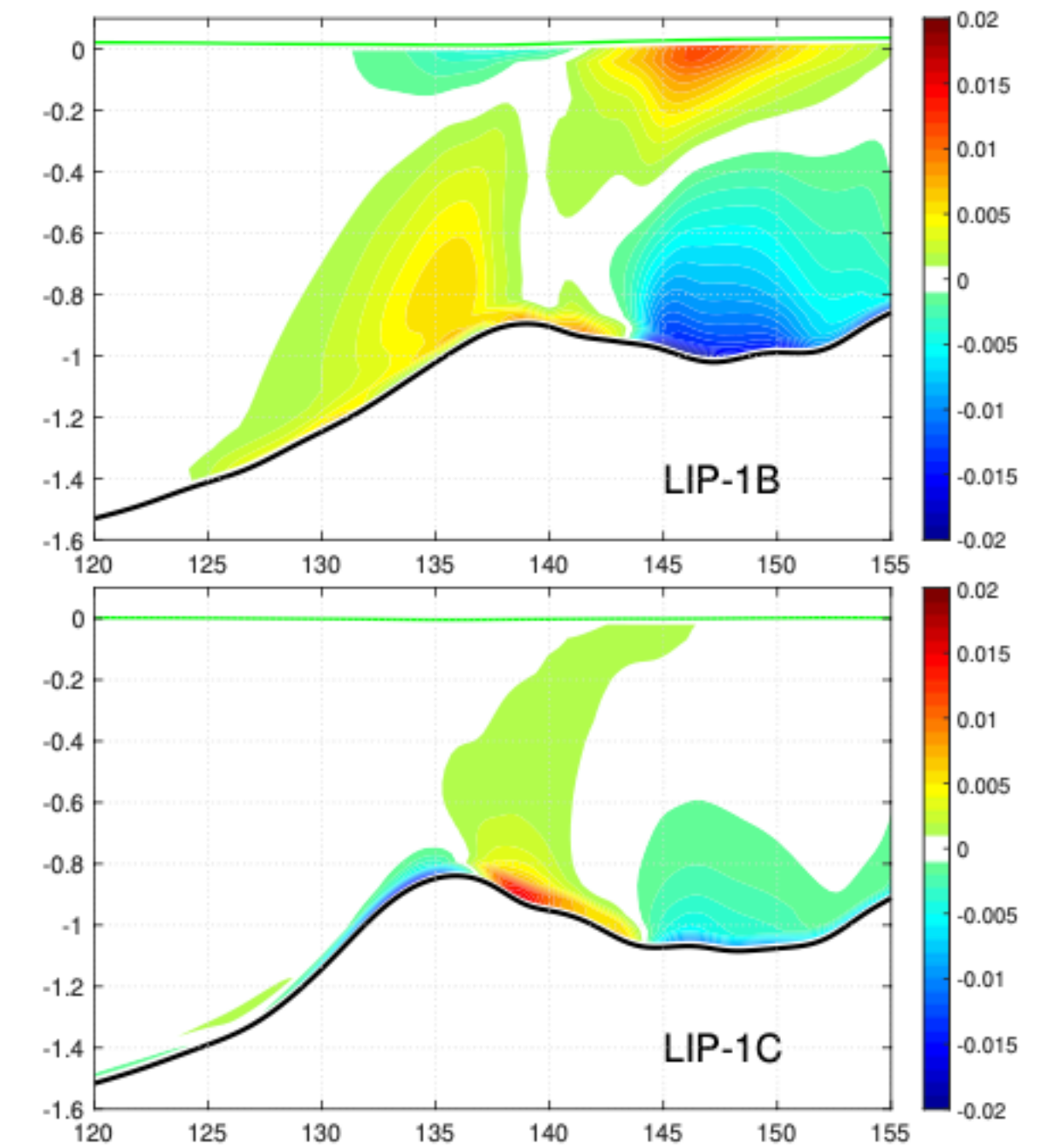
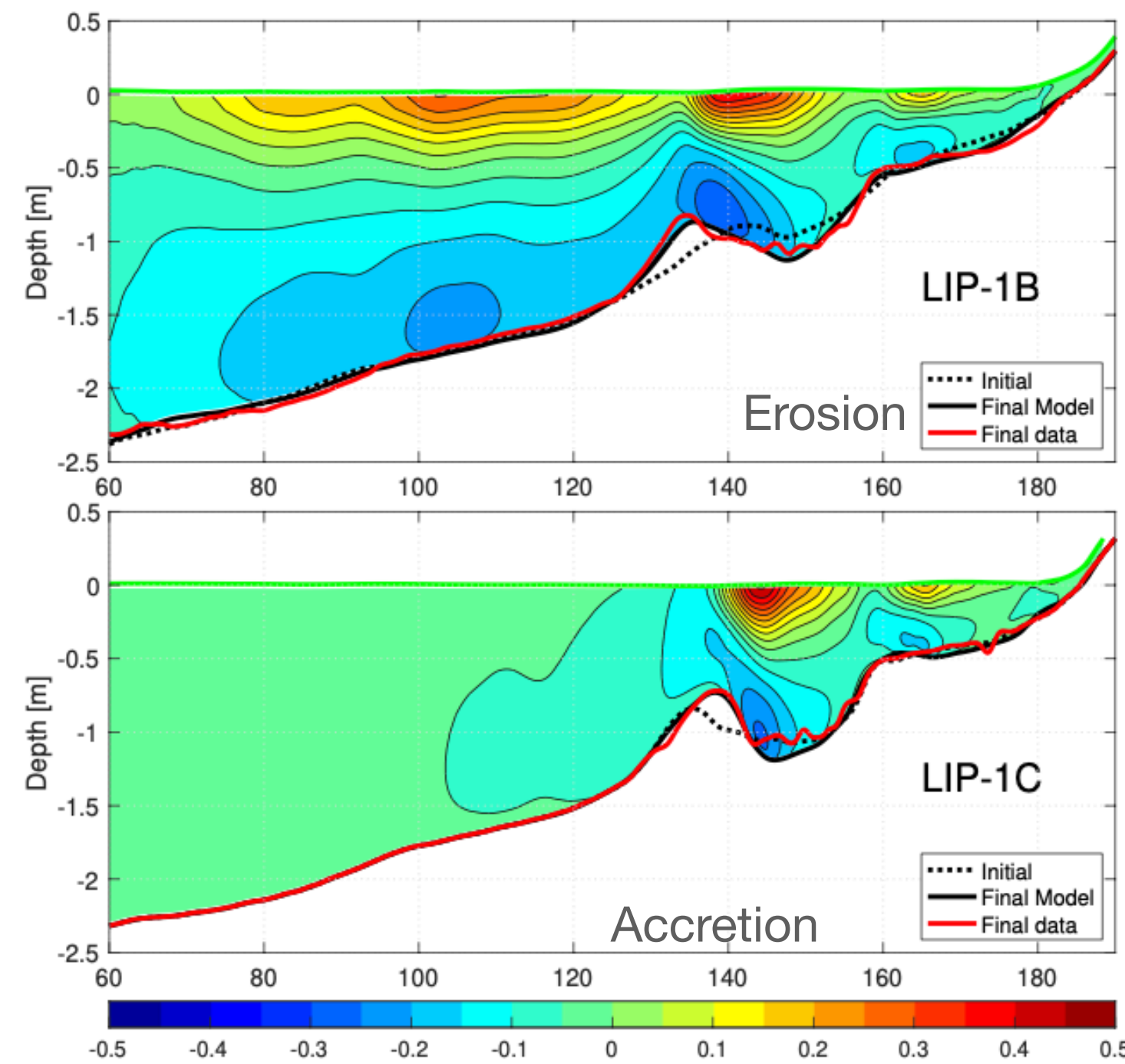
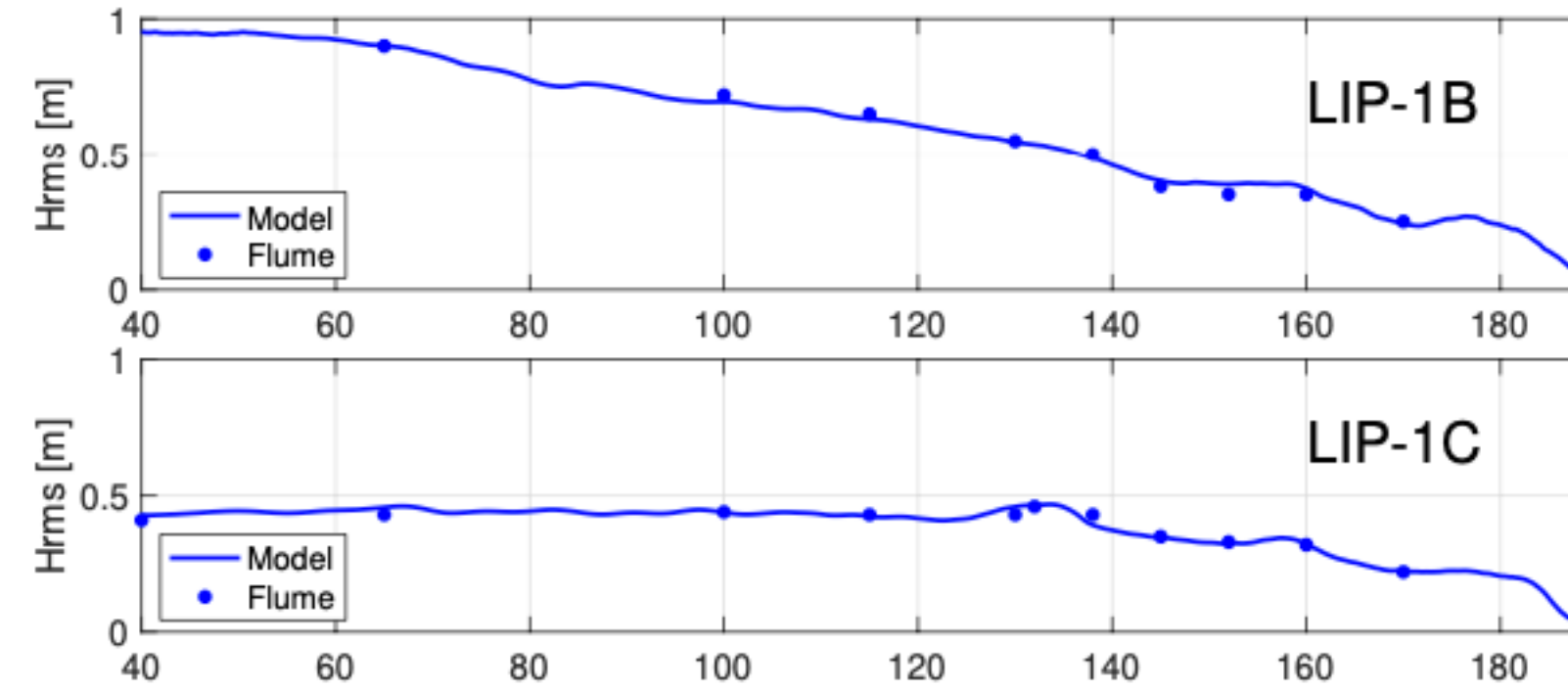
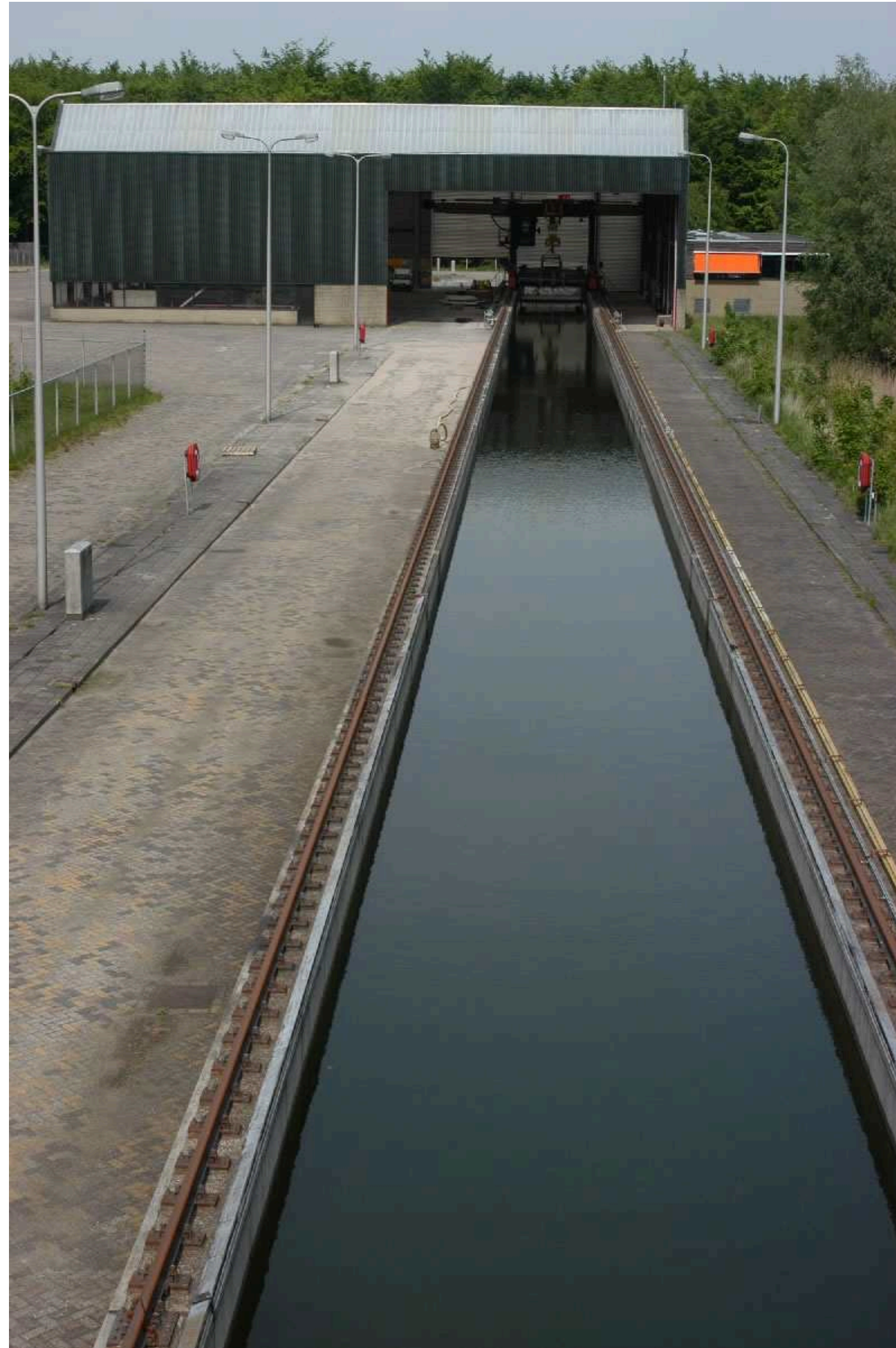
bathymetry



Bed evolution [m]



EXAMPLE 4



SUMMARY

Currently

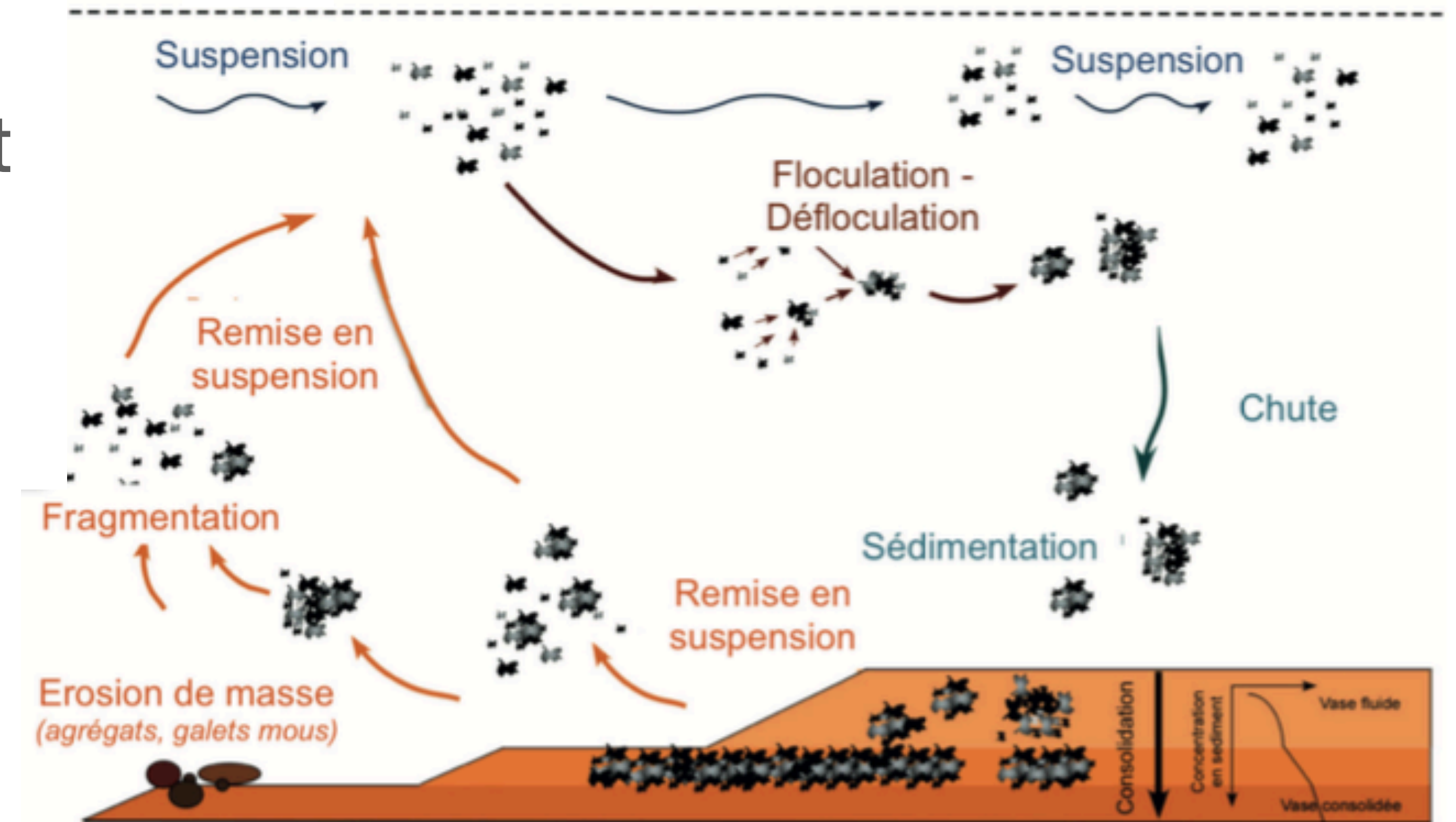
- Increasing effort
- Focus on sandy/wave dominated environment
- More and more confident
- Wave resolved configurations !

Underway

- consolidation
- flocculation

TBD

- interaction with vegetation
- bio diffusion
- Effect on density



Flocculation

- FLOCMOD
- Nombre de classes constant avec transfert entre classes

$$\frac{dN(k)}{dt} = G_a(k) + G_{bs}(k) + G_{bc}(k) - L_a(k) - L_{bs}(k) - L_{bc}(k)$$

Tous les sédiments cohésifs sont traités comme des floccs avec un diamètre caractéristique

Agrégation par collision : cisaillement ou vitesse de chute
 Désagrégation par collision ou turbulence

Différentes fonctions de redistribution

<i>Symbol in Text</i>	<i>Model Variable Name in FLOCMOD</i>	<i>Description</i>	<i>Typical or Default Value</i>	<i>Units</i>
	l_ADS	Enable differential settling	F	True/False
	l_ASH	Enable shear aggregation	T	True/False
D_p	f_dp0	Primary particle size	4e-6	m
	f_dmax	Maximum particle size	Not used	m
	f_nb_frag	Number of fragments by shear erosion	2	-
α	f_alpha	Flocculation efficiency (range: 0 – 1)	0.35	-
β	f_beta	Shear fragmentation rate (0 – 1)	0.15	-
	f_ater	Ternary breakup: 0.5; Binary: 0.0	0.0	-
	f_ero_frac	Fraction of shear fragmentation term transferred to shear erosion (0 – 1)	0.0	-
	f_ero_nbfrag	Number of fragments induced by shear erosion	2.0	-
	f_ero_iv	Fragment size class	1	-
	f_collfragparam	Fragmentation rate for collision-induced breakup	0.01	-
	f_clim	Min. concentration below which floc processes are not calculated	0.001	kg / m ³